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Analytical Development of the Planetary Disturbing  
Function on a Digital Computer

by

I. G. Izsak, B. Benima, and Sara B. Mills

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FUNCTION ON A DIGITAL COMPUTER

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Errata to SAO Special Report No. 140	

ANALYTICAL DEVELOPMENT OF THE PLANETARY DISTURBING  
FUNCTION ON A DIGITAL COMPUTER<sup>1</sup>

by

I. G. Izsak,<sup>2</sup> B. Benima,<sup>3</sup> and Sara B. Mills<sup>3</sup>

Introduction

The purpose of this report is to describe our recently completed IBM 7094 computer program for the analytical development of the planetary disturbing function. Our reason for undertaking this work and the mathematics of the program has already been documented in sufficient detail (Izsak and Benima, 1963; Izsak, Gerard, Efimba, and Barnett, 1964). We are now concerned with implementing the construction of a powerful computational tool that has various applications in celestial mechanics.

A few equations have to be added to those given in SAO Special Report No. 140, and their numbering is continued in this report. There will be a small change in notation. The choice of the indices  $m_1$  and  $m_2$  in the series (30) and in related formulas was unfortunate inasmuch as the same symbols were used to denote the masses of the planets. In this report these indices are marked with  $s_1$  and  $s_2$ . The adopted expansion of the Jacobi coefficients is the classical one (12). In order to assure greater flexibility, our program does not use equations (28) and (29). Instead, the complementary part of the disturbing function is obtained separately from the principal one as follows.

The planetary disturbing function takes slightly different forms depending on the chosen coordinates in the basic differential equations of motion. Such a choice also affects the most convenient definition of orbital elements. Three possibilities of distinct advantage offer themselves: conventional relative coordinates, canonical relative coordinates, and Jacobi's canonical coordinates (Charlier, 1927). Only the first two will be considered here.

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Working with conventional relative coordinates, we need for the perturbations of an inner planet by an outer one the function

$$R = Gm_2 a_2^{-1} \{ a_2 \Delta^{-1} - a_2 r_1 r_2^{-2} \cos \Phi \},$$

and for the perturbations of an outer planet by an inner one

$$R = Gm_1 a_2^{-1} \{ a_2 \Delta^{-1} - a_2 r_2 r_1^{-2} \cos \Phi \},$$

where  $\Delta = (r_1^2 + r_2^2 - 2r_1 r_2 \cos \Phi)^{\frac{1}{2}}$  denotes the mutual distance of the planets, and the expressions in curly brackets are dimensionless. Let us introduce the auxiliary function

$$\rho = \frac{r_1 r_2}{a_1 a_2} \cos \Phi; \quad (68)$$

then we can write

$$- a_2 r_1 r_2^{-2} \cos \Phi = \frac{a_1}{a_2} \frac{\partial^2 \rho}{\partial M_2^2} \quad \text{and} \quad - a_2 r_2 r_1^{-2} \cos \Phi = \left( \frac{a_2}{a_1} \right)^2 \frac{\partial^2 \rho}{\partial M_1^2}.$$

Working with canonical relative coordinates (Poincaré, 1897), we find again  $a_2 \Delta^{-1}$  as the (dimensionless) principal part of the disturbing function. The complementary part, however, turns out to be

$$- \frac{m_0 \sqrt{a_2/a_1}}{\sqrt{m_0+m_1} \sqrt{m_0+m_2}} \frac{\partial^2 \rho}{\partial M_1 \partial M_2},$$

where  $m_0$  stands for the mass of the Sun. This function is the same for the perturbations of the inner and outer planets.

To sum up, the elaboration of a planetary perturbation theory requires in either of these cases the development of the functions  $a_2 \Delta^{-1}$  and  $\rho$  into a multiple Fourier series.

. 1. The principal part

In analogy with equation (31), the development of the function  $a_2 \Delta^{-1}$  is of the form

$$a_2 \Delta^{-1} = \sum_{-\infty}^{\infty} \sum_{-\infty}^{\infty} \sum_{-\infty}^{\infty} \sum_{-\infty}^{\infty} c_{j_1 j_2 k \ell} \cos[j_1 M_1 + j_2 M_2 + (k+\ell)\lambda_1 - (k-\ell)\lambda_2] , \quad (31')$$

whose arguments can also be written as

$$i_1 \lambda_1 + i_2 \lambda_2 - j_1 \omega_1 - j_2 \omega_2 ,$$

where

$$i_1 = j_1 + k + \ell \quad \text{and} \quad i_2 = j_2 - k + \ell .$$

The coefficients  $c_{j_1 j_2 k \ell}$  of the above trigonometric series in turn are power series in the elements  $e_1$ ,  $e_2$ , and  $v = \sin^2(J/2)$ . Their general expressions by means of Laplace coefficients and Newcomb operators were derived in Special Report No. 140. For the sake of easy reference we repeat here some of the equations used in their computation:

$$c_{j_1 j_2 k \ell} = c_{-j_1, -j_2, -k, -\ell} = \sum_{s_1} \sum_{s_2} c_{j_1 j_2 k \ell}^{s_1 s_2} e_1^{s_1} e_2^{s_2} , \quad (30')$$

the summations being extended over all values of the indices  $s_1$  and  $s_2$  for which

$$s_1 = |j_1| + 2h_1 , \quad s_2 = |j_2| + 2h_2 ,$$

and

$$c_{j_1 j_2 k \ell}^{s_1 s_2} = \prod_{j_1 j_2}^{s_1 s_2} (D|k, \ell) b_{k \ell}(\alpha) ; \quad (27')$$

the combined Newcomb operators are defined by

$$\prod_{j_1 j_2}^{s_1 s_2} (D|k, \ell) = \prod_{j_1}^{s_1} (D|k+\ell) \cdot \prod_{j_2}^{s_2} (D|-k+\ell) ; \quad (26')$$

$\alpha = a_1/a_2$ ,  $b_{k\ell}(\alpha) = b_{|k||\ell|}(\alpha)$ , and for  $\ell \geq 0$  the expansion of the Jacobi coefficients in terms of Laplace coefficients is given by

$$b_{k\ell}(\alpha) = \sum_m (-1)^m v^{\ell+m} b_{k\ell m}(\alpha) , \quad (12)$$

where

$$b_{k\ell m}(\alpha) = \left[ \frac{1}{2} \right]_{\ell+m} \sum_{j=0}^m \binom{\ell+m}{j} \binom{\ell+m}{m-j} b_{\frac{1}{2}+\ell+m}^{1+\ell+m} .$$

In other words, we have

$$c_{j_1 j_2 k\ell} = \sum_{s_1 s_2} \sum_s c_{j_1 j_2 k\ell}^{s_1 s_2 s} e_1^{s_1} e_2^{s_2} v^s \quad (69)$$

with

$$s = \ell + m \quad \text{and}$$

$$c_{j_1 j_2 k\ell}^{s_1 s_2 s} = (-1)^m \prod_{j_1 j_2}^{s_1 s_2} (D|k, \ell) b_{k\ell m}(\alpha) . \quad (70)$$

## 2. The complementary part

There is not much to say about the analytical development of such a simple function as  $\rho$ . It is easily obtained from the definition of Hansen coefficients by the expansion (32).

The general form

$$\rho = \sum_{-\infty}^{\infty} \sum_{k, \ell}^{\infty} \gamma_{j_1 j_2 k\ell} \cos[j_1 M_1 + j_2 M_2 + (k+\ell)\lambda_1 - (k-\ell)\lambda_2] \quad (71)$$

of this development is the same as (31'). But because in (68)

$$\cos \Phi = \mu \cos(u_1 - u_2) + v \cos(u_1 + u_2) , \quad (72)$$

$$(r_1/a_1) \exp iu_1 = \sum_{-\infty}^{\infty} x_{j_1+l}^{1,1} z_1^{j_1} \zeta_1 \quad \text{and} \quad (r_2/a_2) \exp iu_2 = \sum_{-\infty}^{\infty} x_{j_2+l}^{1,1} z_2^{j_2} \zeta_2 ,$$

only the following combinations of the indices  $k, \ell$  occur:

$$(k, \ell) = (1, 0), (-1, 0), (0, 1), (0, -1).$$

The coefficients  $\gamma_{j_1 j_2 k \ell}$  are

$$\gamma_{j_1 j_2 10} = \gamma_{-j_1, -j_2, -1, 0} = \frac{\mu}{2} x_{j_1+1}^{1,1} x_{j_2-1}^{1,-1}$$

$$\gamma_{j_1 j_2 01} = \gamma_{-j_1, -j_2, 0, -1} = \frac{\nu}{2} x_{j_1+1}^{1,1} x_{j_2+1}^{1,1}.$$

Thus using the definition

$$x_{j+k}^{n,k}(e) = \sum_m \prod_j^m (n|k) e^m$$

of the Newcomb "operators," we find the expansions

$$2\gamma_{j_1 j_2 10} = \sum_{s_1} \sum_{s_2} \gamma_{j_1 j_2 10}^{s_1 s_2 0} e_1^{s_1} e_2^{s_2} + \sum_{s_1} \sum_{s_2} \gamma_{j_1 j_2 10}^{s_1 s_2 1} e_1^{s_1} e_2^{s_2}, \quad (73)$$

$$2\gamma_{j_1 j_2 01} = \sum_{s_1} \sum_{s_2} \gamma_{j_1 j_2 01}^{s_1 s_2 1} e_1^{s_1} e_2^{s_2},$$

where

$$\begin{aligned} \gamma_{j_1 j_2 10}^{s_1 s_2 0} &= -\gamma_{j_1 j_2 10}^{s_1 s_2 1} = \prod_{j_1}^{s_1} (1|1) \prod_{j_2}^{s_2} (1|-1) \\ \gamma_{j_1 j_2 01}^{s_1 s_2 1} &= \prod_{j_1}^{s_1} (1|1) \prod_{j_2}^{s_2} (1|1). \end{aligned} \quad (74)$$

Then the coefficients in the Fourier series of the (dimensionless) complementary part of the disturbing function are

$$-\alpha^{i_2 i_2} \gamma_{j_1 j_2 k\ell} \quad \text{and} \quad -\alpha^{-2}^{i_1 i_1} \gamma_{j_1 j_2 k\ell}$$

for conventional relative coordinates,

and

(75)

$$\frac{m_0^{\alpha-\frac{1}{2}}}{\sqrt{m_0+m_1} \sqrt{m_0+m_2}} i_1 i_2 \gamma_{j_1 j_2 k\ell}$$

for canonical relative coordinates.

From now on we assume that the principal and complementary parts of the disturbing function have been merged. That is, the c-coefficients are supposed to have been modified so as to include the contribution of the  $\gamma$ -coefficients.

### 3. The pattern of indices

Once the mathematics of the developments (31') and (75) is formulated and the several required subroutines are all coded, our problem consists of organizing the latter into an efficient unity.

The ultimate building elements of the disturbing function depend on seven indices. Each of these indices  $j_1, j_2, k, \ell, s_1, s_2, s$  has a theoretically infinite range. In practical applications, of course, the relevant expansions have to be limited to a finite, although sometimes a very large number of terms. Various circumstances can be used with advantage.

The coefficients  $c_{j_1 j_2 k\ell}$  of our quadruple Fourier series contain the factor  $e_1^{|j_1|} e_2^{|j_2|} v^{\frac{1}{2}|k\ell|}$ . As  $e_1, e_2$ , and  $v^{\frac{1}{2}}$  are small quantities of usually comparable order of magnitude, it is natural to limit the development to those values of the indices,  $j_1, j_2$ , and  $\ell$ , for which

$$p = |j_1| + |j_2| + 2|\ell| ,$$

called the rank of a term, does not exceed a certain preassigned integer  $P$ .

Similarly, with the expansion (69) we associate the integers

$$q = s_1 + s_2 + 2s \leq Q ,$$

and call them the degree of a coefficient  $c_{j_1 j_2 k\ell}^{s_1 s_2 s}$ . Note that  $q-p=2r$  is always a nonnegative even integer. Needless to say, the proper limits  $P$  and  $Q$  depend largely on the pair of planets under consideration.

In general, the Laplace coefficients and their derivatives decrease with increasing absolute values of the index  $k$ . Moreover, the integration of the Fourier series derived from (31') introduces divisors that, as a rule, slowly increase at the same time. (Long-period terms with small divisors constitute a notable exception to this rule. Like the secular terms, they must be treated with special care.) Thus we may also impose a condition  $|k| \leq K$ .

Due to the symmetry in relation (30'), it is sufficient to compute the terms of the disturbing function the indices of which are

$$\begin{array}{llll}
 j_1 = 0 & j_2 = 0 & \ell = 0 & (p = 0) & k = 0 \\
 j_1 = 0 & j_2 = 0 & \ell = 0 & (p = 0) & k = 1, \dots, K \\
 j_1 > 0 & j_2 = 0 & \ell = 0 & (p = j_1 = 0, \dots, P) & k = -K, \dots, K \\
 & j_2 > 0 & \ell = 0 & (p = |j_1| + j_2 = 0, \dots, P) & k = -K, \dots, K \\
 & \ell > 0 & (p = |j_1| + |j_2| + 2\ell = 0, \dots, P) & k = -K, \dots, K
 \end{array}$$

If the terms belonging to these indices are known, then the complete expression (31') in the range  $p \leq P$ ,  $|k| \leq K$  is obtained by taking twice all the terms just specified, except the first one, which is a constant.

Let us give a concrete example. The 98 solutions of the inequality  $|j_1| + |j_2| + 2\ell \leq 6$  in question are:

$j_1$	$j_2$	$\ell$									
0	0	0	0	4	0	0	3	1	4	0	1
			-1	3	0	-1	2	1	3	1	1
1	0	0	-2	2	0	-2	1	1	2	2	1
0	1	0	-3	1	0	-3	0	1	1	3	1
			2	0	1	-2	-1	1	0	4	1
2	0	0	1	1	1	-1	-2	1	-1	3	1
1	1	0	0	2	1	0	-3	1	-2	2	1
0	2	0	-1	1	1	1	-2	1	-3	1	1
-1	1	0	-2	0	1	2	-1	1	-4	0	1
0	0	1	-1	-1	1	1	0	2	-3	-1	1
			0	-2	1	0	1	2	-2	-2	1
3	0	0	1	-1	1	-1	0	2	-1	-3	1
2	1	0	0	0	2	0	-1	2	0	-4	1
1	2	0							1	-3	1
0	3	0	5	0	0	6	0	0	2	-2	1
-1	2	0	4	1	0	5	1	0	3	-1	1
-2	1	0	3	2	0	4	2	0	2	0	2
1	0	1	2	3	0	3	3	0	1	1	2
0	1	1	1	4	0	2	4	0	0	2	2
-1	0	1	0	5	0	1	5	0	-1	1	2
0	-1	1	-1	4	0	0	6	0	-2	0	2
			-2	3	0	-1	5	0	-1	-1	2
4	0	0	-3	2	0	-2	4	0	0	-2	2
3	1	0	-4	1	0	-3	3	0	1	-1	2
2	2	0	3	0	1	-4	2	0	0	0	3
1	3	0	2	1	1	-5	1	0			
			1	2	1						

To find the appropriate indices  $s_1$ ,  $s_2$ ,  $s$  we recall that

$$s_1 = |j_1| + 2h_1, \quad s_2 = |j_2| + 2h_2, \quad \text{and} \quad s = \ell + m,$$

so that

$$h_1 + h_2 + m = r \leq \frac{1}{2}(Q-p) .$$

For example, corresponding to the choice  $P = 6$  and  $Q = 8$ , we get:

$$\begin{array}{l} p = 0 \\ r = 4 \end{array}$$

$h_1$	$h_2$	$m$
0	0	0
1	0	0
0	1	0
2	0	0
1	1	0
0	2	0
3	0	0
2	1	0
1	2	0
0	3	0
4	0	0
3	1	0
2	2	0
1	3	0
0	4	0
0	0	1
1	0	1
0	1	1
2	0	1
1	1	1
0	2	1
3	0	1
2	1	1
1	2	1
0	3	1
0	0	2
1	0	2
0	1	2
2	0	2
1	1	2
0	2	2
0	0	3
1	0	3
0	1	3
0	0	4

$$\begin{array}{l} p = 1, 2 \\ r = 3 \end{array}$$

$h_1$	$h_2$	$m$
0	0	0
1	0	0
0	1	0
2	0	0
1	1	0
0	2	0
3	0	0
2	1	0
1	2	0
0	3	0
4	0	0
3	1	0
2	2	0
1	3	0
0	4	0
0	0	1
1	0	1
0	1	1
2	0	1
1	1	1
0	2	1

$$\begin{array}{l} p = 3, 4 \\ r = 2 \end{array}$$

$h_1$	$h_2$	$m$
0	0	0
1	0	0
0	1	0
2	0	0
1	1	0
0	2	0
3	0	0
2	1	0
1	2	0
0	3	0
4	0	0
3	1	0
2	2	0
1	3	0
0	4	0
0	0	1
1	0	1
0	1	1
2	0	1
1	1	1
0	2	1

$$\begin{array}{l} p = 5, 6 \\ r = 1 \end{array}$$

$h_1$	$h_2$	$m$
0	0	0
1	0	0
0	1	0
0	0	1

The size of the individual coefficients is in reality much less regular than the foregoing general remarks would seem to indicate. Human judgment as to which terms should be kept and which neglected is here probably preferable to computer-made decisions. The efficient use of the present program is facilitated by the following features. First, for each combination of the  $j_1, j_2, \ell$  indices we specify separately the degree  $q$  of the coefficients to be retained, as well as an interval  $\underline{k} \leq k \leq \bar{k}$  of the index  $k$ . Second, the program can be run in two modes, namely either to compute the coefficients  $c_{j_1 j_2 k \ell}^{s_1 s_2 s}$ , or to evaluate the monomials  $c_{j_1 j_2 k \ell}^{s_1 s_2 s} e_1^{l_1} e_2^{l_2} v^s$ . This way we get a fair idea about the convergence of the analytical development of the disturbing function in any particular case. Third, the effect of the divisors of integration is also exhibited. We shall say more about the program in Part 4.

Since the quantities  $n_1, n_2$  are the mean motions of the two planets, the angular frequency of a term in the Fourier series (31') is approximately  $i_1 n_1 + i_2 n_2$ . It is therefore of interest to know which indices  $j_1, j_2, k, \ell$  can give rise to a certain combination

$$i_1 = j_1 + k + \ell \quad \text{and} \quad i_2 = j_2 - k + \ell .$$

These relations are equivalent to

$$j_1 + j_2 + 2\ell = i_1 + i_2 , \quad (76)$$

$$j_1 - j_2 + 2k = i_1 - i_2 . \quad (77)$$

For a given pair of indices  $i_1, i_2$  equation (76) has an infinite number of solutions. But we are interested only in solutions with rank  $p \leq P$ , and these are finite in number. Indeed, the indices  $j_1, j_2, \ell$  satisfying the conditions (76) and  $|j_1| + |j_2| + 2|\ell| \leq P$  are:

$$\ell = -[v/2], \dots, [u/2] - 1, [u/2] ,$$

$$(j_1, j_2) = ([u] - 2\ell, -[v]) , \dots , (-[v], [u] - 2\ell) \quad \text{if } \ell \geq 0 ,$$

$$(j_1, j_2) = ([u], -[v] - 2\ell) , \dots , (-[v] - 2\ell, [u]) \quad \text{if } \ell < 0 ,$$

with

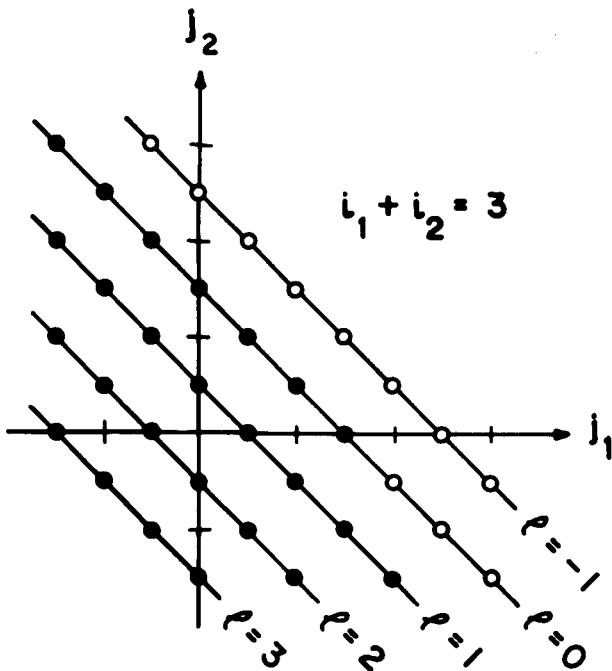
$$u = \frac{1}{2}(P + i_1 + i_2) \geq 0 \quad \text{and} \quad v = \frac{1}{2}(P - i_1 - i_2) \geq 0 .$$

Once a pair  $(j_1, j_2)$  has properly been chosen, the value of the index  $k$  is determined by equation (77). It is sufficient to obtain the quadruples  $(j_1, j_2, k, \ell)$  under the condition  $i_1 + i_2 \geq 0$ ; whenever the convention adopted on p. 7 is violated, we simply change signs, except in the case  $i_1 + i_2 = 0$ , where the quadruples violating our convention can be disregarded.

As an example, let us consider the great inequality in the theories of Jupiter and Saturn associated with the arguments

$$-2\lambda_1 + 5\lambda_2 - j_1 w_1 - j_2 w_2 .$$

Due to their small divisors, such terms of the disturbing function must be carried up to an exceptionally high rank. Put  $P = 9$ , so that  $u = 6$ ,  $v = 3$ . The appropriate solutions of equation (76) are exhibited in the following figure, where open circles indicate that the sign of the corresponding indices is to be changed.



#### 4. The program

##### Introduction

The program is written in FORTRAN II for the IBM 7094 computer and double-precision arithmetic is used. It computes the coefficients

$c_{j_1 j_2 k \ell}^{s_1 s_2 s}$  (70) of the Fourier expansion of the disturbing function by applying

the combined Newcomb operators (see Special Report No. 140) to the Jacobi coeffi-

clients which are derived from the Laplace coefficients (see Special Report No.129).

It also gives the first and second derivatives DC and  $D^2C$ , where  $D = \alpha \frac{\partial}{\partial \alpha}$  and  $C = c_{j_1 j_2 k \ell}^{s_1 s_2 s}$ , and the fractions  $C/N$ ,  $DC/N$ , and  $C/N^2$ , where  $N = i_1 + \beta i_2$ .

A second mode is provided that computes the monomials  $c_{j_1 j_2 k \ell}^{s_1 s_2 s} e_1^{s_1} e_2^{s_2} v^s$  (69).

The complementary parts are computed in conventional relative coordinates (inner or outer planets), or in canonical relative coordinates as specified by the user.

### Program limitations

There are two versions of the program. The first and smaller version requires 13356 cells of lower core and 3341 cells of common storage. The limitations of this version are:

$$|k| \leq 15, \ell \geq 0 \quad \text{for } k \text{ and } \ell \text{ in } c_{j_1 j_2 k \ell}^{s_1 s_2 s},$$

the degree  $q \leq 8$ ,

the rank  $p \leq 6$ .

The second version requires 15360 cells of lower core and 6305 cells of common storage. Here the limitations are:

$$|k| \leq 20, \ell \geq 0, q \leq 10, \text{ and } p \leq 9.$$

### Method

First the Laplace coefficients  $D_{b_k}^{j_1 s+1}$  are computed and stored for later use. Next we generate the inner and outer Newcomb operators and store the coefficients of these polynomials. The program then reads in the parameters  $j_1, j_2, \ell$ , the minimum and the maximum limits of  $k$ , and the degree  $q$  of the coefficients  $c_{j_1 j_2 k \ell}^{s_1 s_2 s}$  we want to compute.

All possible combinations of  $s_1, s_2$ , and  $s$  for the given parameters  $j_1, j_2, \ell$ , and  $q$  are computed and stored. Then for each  $k$  from  $k_{\min}$  to  $k_{\max}$  and for each combination of  $s_1, s_2$ , and  $s$  we recall from storage the corresponding inner and outer Newcomb operators  $\prod_{j_1}^{s_1} \prod_{j_2}^{s_2}$  and evaluate them for the current values of  $(k+\ell)$  and  $(-k+\ell)$ , respectively (26'). The two resulting polynomials in the differential operator  $D$  are multiplied together. The product polynomial is the combined operator  $\prod_{j_1 j_2}^{s_1 s_2}$  (26'). Next the  $b_{k \ell m}$  and all its required derivatives are determined for each new  $m$ . Finally we apply the combined operator to the  $b_{k \ell m}$  (70).

If the  $c_{j_1 j_2 k \ell}^{s_1 s_2 s}$  have to be evaluated for a very large number of indices, it is more efficient to compute all the possible combinations of the  $b_{k \ell m}$  directly after the computation of the Laplace coefficients, storing them for later use. In the smaller version of the program this would require an extra 1200 locations.

Because of the symmetry  $c_{j_1 j_2 k \ell} = c_{-j_1, -j_2, -k, -\ell}$  (30') we evaluate

only half of the coefficients and then multiply each of them by two except the  $c_{0000}$ . To avoid duplication, we adopt the convention that  $\ell$  is always greater than or equal to zero and if  $\ell = 0$  then  $j_2 \geq 0$ . If this convention is violated we simply reverse the signs of all four indices.

If  $|k| + \ell = l$  and the coefficients of the complementary parts in formula (75) are nonzero then we compute the complementary parts of the  $c$ -coefficients in the coordinates specified by the user in the input and add them to the principal parts. In these cases the printout is preceded by an asterisk.

### Usage

The first data card should contain six control characters for the printing of intermediate results using the format (6I10). They control the printing of the Laplace coefficients, the inner and the outer J's, the inner and the outer X's (Special Report No. 140), and the time used by the program, in that order. A blank card will suppress the printing of all intermediate results.

Each group of input cards with indices must be preceded by a control card which indicates the mode and the choice of coordinates and gives the values of the program parameters. The first character on a control card should be either a 'C' for coefficients or a 'M' for monomials followed by a 1, 2, or 3 for conventional relative coordinates, inner or outer planet, or canonical relative coordinates, respectively. The values for  $\alpha (0 < \alpha = a_1/a_2 < 1)$  and  $\beta (0 < \beta = n_2/n_1 < 1)$  follow, and if monomials are requested, the values for  $e_1, e_2$ , and  $\sqrt{v} (= \sin J/2)$ . Finally, if canonical relative coordinates were specified,  $m_0/m_1$  and  $m_0/m_2$ . The control cards are in free-field format, and numerals are defined by a trailing blank.

This control card is followed by a group of parameter cards, each card containing  $j_1$ ,  $j_2$ ,  $\ell$ ,  $k_{\min}$ ,  $k_{\max}$ , and  $q$  with a format of (6I10). For each  $j_1$ ,  $j_2$ ,  $k$ , and  $\ell$  where  $k$  runs through all the integral values from  $k_{\min}$  to  $k_{\max}$ , all the combinations of  $s_1$ ,  $s_2$  and  $s$  such that  $s_1 + s_2 + 2s \leq q$  are generated. For every set of indices  $s_1$ ,  $s_2$ ,  $s$ ,  $j_1$ ,  $j_2$ ,  $k$ ,  $\ell$ , the coefficient  $c_{j_1 j_2 k \ell}^{s_1 s_2 s}$ , its first two Newcomb derivatives, and the fractions C/N, DC/N, and  $C/N^2$  are evaluated and printed out. If the value for  $q$  is preceded by a minus sign on the input card, the printout will be suppressed.

To end a group of parameter cards a blank card is inserted. The program then reads a new control card for the next group of parameter cards. In order to terminate the program a card with a zero or a decimal point is placed directly after the blank card.

We shall now discuss the MAIN program and the subroutines that have not already been described in the Special Reports Nos. 129 and 140.

#### MAIN program

After the necessary initializations and the reading of the print-control card, the MAIN program reads the first control card into a buffer. The program will exit if the coordinate code number is zero. Hence a card with a zero or a decimal point in the place of a control card will terminate the program. A blank card may not be used since the numerals on the control card are read in a free-field format. If the coordinate code number is not zero, the first character of the control card image is read from the buffer. If this character is neither a 'M' or a 'C' an error message is returned and the program exits. If it is a 'C' the card is read for the second time from the buffer and  $\alpha$ ,  $\beta$ ,  $m_1$ , and  $m_2$  are picked up. For monomials, i.e., in case of a 'M',  $\alpha$ ,  $\beta$ ,  $e_1$ ,  $e_2$ ,  $\sqrt{v}$ ,  $m_1$ , and  $m_2$  are read and the coordinate control code is set negative. The program then calls the subroutine MORCOE to compute and store the Laplace coefficients. If the first print control is greater than zero, the Laplace coefficients are printed out. Next the subroutine COMBOP is called to develop the inner and outer Newcomb operators and store them in two linear arrays. The appropriate headings are written according to the choice of coordinates. If the coordinate code is negative, i.e., if monomials were requested, the values of  $e_1$ ,  $e_2$ , and  $v$  are printed out and their powers are computed and stored.

The program now proceeds to read a parameter card with  $j_1$ ,  $j_2$ ,  $\ell$ ,  $k_{\min}$ ,  $k_{\max}$ , and  $q$  using the format (6I10). Compliance with the program limitations is checked, and if not satisfied an error message is returned.

The subroutine INDEX finds and stores all possible combinations of  $s_1$ ,  $s_2$ , and  $s$  for the given set of parameters. The program ends with a loop in which  $k$  is stepped up from  $k_{\min}$  to  $k_{\max}$ . For each  $k$  and each combination of  $s_1$ ,  $s_2$ , and  $s$  the subroutine SOLVE is called to compute and print the  $c_{j_1 j_2 k l}^{s_1 s_2 s}$ .

The program then goes back and reads the next parameter card. If a blank parameter card is encountered, the page line count is reset and a new control card is read in. If the new  $\alpha$  differs from the previous one, the Laplace coefficients are computed again for the new  $\alpha$ .

#### MORCOE

The subroutine MORCOE first computes the Laplace coefficients for  $s + \frac{1}{2} = \frac{1}{2}$  by calling LPLCOF. This program LPLCOF is described in detail in Special Report No. 129 and is used here essentially unchanged except for dimensions and storage arrangement.

All the results of LPLCOF are stored in the common area and are later overwritten by the results of the Newcomb operator program. MORCOE then computes the Laplace coefficients  $D^j b_k^{s+\frac{1}{2}}$  from  $s + \frac{1}{2} = \frac{1}{2}$  to  $s + \frac{1}{2} = \frac{41}{2}$  by recursion and stores the results in lower core for later use by the BKLM program.

Using formula (16) in Special Report No. 129 we compute  $D^j b_k^{s+\frac{1}{2}}$  for  $s = 1, 2, 3, 4$ , and  $j = 0, \dots, Q - 2s + 2$ , first for  $k = 0$  (taking  $D^j b_{-1}^{s+\frac{1}{2}} = D^j b_1^{s+\frac{1}{2}}$ ) and then for  $k = 1, \dots, 19$  (smaller version).

#### COMBOP

The subroutine COMBOP constructs the inner and outer Newcomb operators and stores their coefficients for later use in two linear arrays AICM and ATEMP, respectively.

It does so by calling the Newcomb operator program written at M.I.T. and described in the second part of Special Report No. 140. We have adapted this program to fit our needs. We were mainly concerned with storage limitations and made some changes of which the more important are the following. The numbers in column 16 of array AICT on the bottom of page 30 (Special Report No. 140) were eliminated. This made it possible to store the coefficients of all inner and outer operators up to degree 8 in two arrays AICM and ATEMP each of only 625 double words. These two arrays occupy the same space in the common area that was used previously for all the intermediate results of the Laplace coefficients program. The PRINT routine was

simplified, and INTERVAL was eliminated. The routines GETAS, GETPSI, and BIGPSI are not needed for the present application. We added the routine OUTRJS which constructs the outer J's from the inner J's by substituting (-D-1) for D (page 14, Special Report No. 140) which is accomplished by the subroutine NSUBST. The outer J's are stored in ATEMP. The subroutines STORE and KEEP are combined to one routine and modified so that it now can service both arrays AICM and ATEMP. The subroutines TRANS and DIVIDE are similarly changed.

After calling GETJS, COMBOP calls OUTRJS and then twice GETXS, once with AICM as argument and the second time with ATEMP to produce the inner and outer X's. The X-arrays overwrite the J-arrays in storage.

Having generated and stored the Laplace coefficients and the inner and outer Newcomb operators, we are ready to enter the inner loop of the program

which computes and prints the  $c_{j_1 j_2}^{s_1 s_2}$  for each set of indices.

### OUTRJS

OUTRJS moves each inner J to the working array AICT with the subroutine TRANS, then converts it with NSUBST to the corresponding outer J and stores this outer J in the array ATEMP.

### NSUBST

The subroutine NSUBST constructs each element of the outer J-array by multiplying each element of the same or higher degree in D in the same k-column of the inner J-array by the proper coefficient of the Pascal triangle, which triangle was stored during the development of the Newcomb operators, and by the proper alternating sign and then adding these products together.

### INDEX

The subroutine INDEX generates all combinations of  $s_1$ ,  $s_2$ , and  $s$  according to the scheme on page 8 and stores the resulting sets in a two-dimensional array. The routine consists of three loops. The total number of combinations  $s_1$ ,  $s_2$ , and  $s$  for each set of indices is also returned to the MAIN program.

### SOLVE

The subroutine SOLVE has two functions, the computation and the printing of the coefficients  $c_{j_1 j_2}^{s_1 s_2}$ .

The format for the headings is constructed during execution time. The spacing of the coefficients of the cosine argument is handled by a subroutine FORMAT. If the divisor  $N = i_1 + \beta i_2$  is zero, only the first half of the heading is printed and three columns instead of six are written out.

If  $|k| + \ell = 1$  and the coefficients of the  $\gamma$ -components (75) belonging to the selected coordinate system are nonzero, then there will be a complementary part. The format is adjusted so that the heading is preceded by an asterisk and a flag is set for the computation of the complementary part. A running line count is kept lest the headings are split over two pages.

After the headings are written out, the coefficients are computed in a loop that is repeated for each combination of  $s_1$ ,  $s_2$ , and  $s$ . The first time through the loop and each time  $m$  changes, the  $b_{klm}$  and its derivatives are evaluated by the subroutine BKLM from the Laplace coefficients. The appropriate combined Newcomb operator now is produced by the subroutine COMBIN in the form of a polynomial in  $D$ . The subroutine APPLY then applies this combined operator to the proper derivatives of  $b_{klm}$  to yield the

$c_{j_1 j_2 k \ell}^{s_1 s_2 s}$  (70), the  $D c_{j_1 j_2 k \ell}^{s_1 s_2 s}$ , and the  $D^2 c_{j_1 j_2 k \ell}^{s_1 s_2 s}$ . Because of the symmetry in (30') the coefficients are doubled except for the  $c_{0000}^{s_1 s_2 s}$  and then divided by  $N$  and  $N^2$ .

If the flag for a complementary part is set, the value of  $s$  is checked. If  $s$  is greater than one, the flag is erased. But if  $s = 0$  or  $s = 1$ , the

function program GAMMA computes  $\pm \prod_{j_1}^{s_1} (1|1) \prod_{j_2}^{s_2} (1|\pm 1)$  and depending on

which coordinate-system was selected,  $\gamma$  then is multiplied by the relevant factor in (75). The complementary part and its first and second derivatives are added to the corresponding principal parts. In case of monomials all

coefficients and quotients are multiplied by  $e_1^{s_1} e_2^{s_2} v^s$ .

After the final loop is satisfied, control is returned to the MAIN program to pick up a new set of indices.

### FORMAT

This function subprogram checks each coefficient in the cosine argument. If it is positive a + sign is inserted in the format. Proper spacing is provided depending on whether the integers have one or two digits.

### BKLM

Using the binomial coefficients computed by the Newcomb operator program and the Laplace coefficients computed by MORCOE, the terms of the sum in (12) are evaluated and summed. The sum is then multiplied by  $\left[ \frac{1}{\ell+m} \right]$  and given the

sign from formula (70). This is repeated for all derivatives up to degree  $(q-2s+2)$ .

#### COMBIN

This subroutine moves the inner Newcomb operator

$$\prod_{j_1}^{s_1}$$

from the linear array AICM to the working array AICT. If  $j_1$  happens to be negative, we change first the signs of  $j_1$ ,  $k$ , and  $\ell$ , using the equality (33), since the Newcomb operators were constructed only for  $\rho \geq \sigma$  in view of the symmetry relation (33) or (37) of Special Report No. 140. It then calls the subroutine EVALUK which evaluates this polynomial by substituting for  $k$  the current numerical value of  $k+\ell$ . The same procedure is followed for the outer operator

$\prod_{j_2}^{s_2}$  except that this time the polynomial is evaluated for the value  $(-k+\ell)$ .

The subroutine MPPOLY multiplies the two polynomials in D and stores the resulting combined operator. Control then is returned to the SOLVE program.

#### EVALUK

Subroutine EVALUK simply multiplies each element of the array AICT by the proper power of the constant  $k+\ell$  for the inner operators and  $-k+\ell$  for the outer operators, and sums the products in each row.

#### MPPOLY

MPPOLY multiplies the two polynomials that resulted from the two calls to EVALUK. It first establishes the degree of the product polynomial. Then each term of the product polynomial is assembled by forming all products that contribute to this term and summing these products. They are found by stepping up the degree of the term in the first polynomial and stepping down the degree in the second polynomial, thus keeping the sum of the degrees constant and equal to the degree of the term of the product polynomial being assembled.

#### APPLY

The subroutine APPLY multiplies each numerical coefficient of the combined operator with the corresponding derivative of  $b_{klm}$  and with the first and second higher derivatives. Each of these products is summed into its

previous total to form  $c_{j_1 j_2 k l}^{s_1 s_2 s}$ ,  $D c_{j_1 j_2 k l}^{s_1 s_2 s}$ , and  $D^2 c_{j_1 j_2 k l}^{s_1 s_2 s}$

## GAMMA

To compute the  $\gamma$ 's of formula (74) for the complementary part, we first check the value of  $k$ . If  $k$  is nonzero,  $|k|$  must be one and  $\ell$  must be zero. Otherwise an error message is returned. If  $k$  is negative we change the signs of  $j_1$ ,  $j_2$ , and  $k$ . Then we evaluate  $\prod_{j_1}^{s_1} (1|1)$  and  $\prod_{j_2}^{s_2} (1|-1)$  with the function routine PI and multiply them together. If  $s = 0$ , we return. If  $s = 1$ , we change sign. In case  $k = 0$ , we check if  $\ell = 1$  and  $s = 1$ . If this is true, we compute  $\gamma = \prod_{j_1}^s (1|1) \prod_{j_2}^{s_2} (1|1)$ . All other cases result in an error message and exit from the program.

## PI

PI evaluates  $\prod_{j_1}^{s_1} (1|1)$  and  $\prod_{j_2}^{s_2} (1|-1)$ . If a  $j$  is negative, we change the sign of  $j$  and of  $k$ , using the relation (33). Then with equation (36') we find  $\prod_j^s$  from the inner X-array and move it to AICT with the routine TRANS.

We add all elements of each column and then add these column totals, if  $k = 1$ . Or if  $k = -1$ , we form an alternating sum.

Immediately following the references, we give two print-out samples of the program. They both pertain to the planets Jupiter and Saturn. Appendix I presents (in mode C) a somewhat more extended development of the disturbing function than Leverrier's classical one in the Annales de l'Observatoire de Paris, vol. 10, p. 68 and pp. 72-93. It was produced by the smaller version of our program; the required machine-time was about one minute. Appendix II exhibits (in mode M) the secular terms and the long-period terms of the great inequality up to the 9th powers of the eccentricities, whenever necessary to conform with modern standards of accuracy.

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Appendix I

THIS  
COMPUTER RUN  
IS DEDICATED  
TO THE MEMORY OF

U.-J. LE VERRIER

(1811-1877)

## SAO ANALYTICAL DEVELOPMENT OF THE PLANETARY DISTURBING FUNCTION

CONVENTIONAL RELATIVE COORDINATES, INNER PLANET

ALPHA = .5454323      BETA = .4026858

8U+J(K,L) COS(I,L+IL-J,M-J,M)

	C	DC	<sup>2</sup> D C	C/N	DC/N	C/N=N
8S+S S S I 1 2	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---

8 O. O6 O. O3 COS(I+OL+OL+OM+OM)

	C	DC	<sup>2</sup> D C
8 O. O6 O. O3 8 2. O6 O. O3 8 O. 26 O. O3 8 4. O6 O. O3 8 2. 26 O. O3 8 0. 46 O. O3 8 6. O6 O. O3 8 4. 46 O. O3 8 2. 26 O. O3 8 0. 66 O. O3 8 0. O6 1. O3 -8.6921352E-01 8 2. O6 1. O3 -4.6224038E-00 8 0. 26 1. O3 -4.6224038E-00 8 4. O6 1. O3 -9.4314108E-00 8 2. 26 1. O3 -6.4137527E-01 8 0. 46 1. O3 -2.4944595E-01 8 0. O6 2. O3 4.1878770E-00 8 2. O6 2. O3 6.1824285E-01 8 0. 26 2. O3 6.1824285E-01 8 0. O6 3. O3 -2.4686431E-01	1.0901658E-00 2.1730330E-01 2.1730330E-01 1.1996160E-01 1.1556209E-00 5.6650056E-01 9.4474330E-02 2.3578527E-00 6.2371487E-00 1.6852656E-00 -8.6921352E-01 -4.6224038E-00 -4.6224038E-00 -9.4314108E-00 -6.4137527E-01 -2.4944595E-01 4.1878770E-00 6.1824285E-01 6.1824285E-01 -2.4686431E-01	2.2065981E-01 7.8442622E-01 7.8442622E-01 9.3373426E-01 7.1807815E-00 3.0488696E-00 1.1488470E-00 2.4533773E-01 5.4807341E-01 1.2650127E-01 -3.1377049E-00 -2.8723126E-01 -2.8723126E-01 -9.8135091E-01 -6.0600578E-02 -2.1922936E-02 2.7154273E-01 5.9164422E-02 5.9164422E-02 -9.3945815E-00	6.4855371E-01 3.8380575E-00 3.8380575E-00 8.4976785E-00 5.6956745E-01 2.1899725E-01 1.5457093E-01 2.9289563E-02 5.8165933E-02 1.20644836E-02 -1.5352230E-01 -2.2782698E-02 -2.2782698E-02 -1.1715825E-03 -6.7686129E-03 -2.3266374E-03 2.2015087E-02 6.6546993E-03 6.6546993E-03 -2.8108789E-03

8 O. O6 1. O3 COS(I+IL-IL+OM+OM)

	C	DC	<sup>2</sup> D C	C/N	DC/N	C/N=N
8 O. O6 1. O3 8 2. O6 1. O3 8 O. 26 1. O3 8 4. O6 1. O3 8 2. 26 1. O3 8 0. 46 1. O3 8 0. O6 1. O3 8 2. O6 1. O3 8 0. 26 1. O3 8 0. O6 2. O3 7.5381742E-02 2.4643393E-01 2.4643393E-01 1.2715741E-01 1.6728477E-00 8.3955046E-01 -1.2118809E-00 -7.4306928E-00 -7.4306928E-00 8.7525085E-00	2.6368667E-01 1.1508800E-00 1.1508800E-00 1.3395223E-00 1.1337164E-01 5.1792204E-00 -5.3945815E-00 -5.0801296E-01 -5.0801296E-01 5.2215863E-01	1.0235760E-01 6.5262463E-00 6.5262463E-00 1.4024265E-01 1.0064119E-02 3.9655412E-01 -2.9175713E-01 -4.2214348E-02 -4.2214348E-02 4.2969331E-02	1.2620115E-01 4.1257001E-01 4.1257001E-01 2.1288195E-01 2.8006161E-02 1.4055424E-00 -2.0288835E-00 -1.2440174E-01 -1.2440174E-01 1.2978945E-01	4.4145388E-01 1.9267588E-00 1.9267588E-00 2.2425757E-00 1.9817315E-01 8.6708475E-00 -9.0313966E-00 -8.5049536E-01 -8.5049536E-01 8.7417749E-01	2.1128102E-01 6.9070852E-01 6.9070852E-01 3.5639846E-01 4.6886815E-00 2.3531040E-00 -3.3966772E-00 -2.0826851E-01 -2.0826851E-01 2.1720841E-01	

8 O. O6 2. O3 COS(I+2L-2L+OM+OM)

	C	DC	<sup>2</sup> D C	C/N	DC/N	C/N=N
8 O. O6 2. O3 8 2. O6 2. O3 8 O. 26 2. O3 8 4. O6 2. O3 8 2. 26 2. O3 8 0. 46 2. O3 8 0. O6 2. O3 8 2. O6 2. O3	2.5776796E-01 -4.6758116E-01 -4.6758116E-01 3.1169384E-01 2.2093487E-00 6.5585296E-01 -1.2228911E-00 -3.2264216E-00	6.0300775E-01 -5.46167466E-01 -5.46167466E-01 1.0901857E-00 9.9820144E-00 3.8561121E-00 -5.0693944E-00 -3.3427961E-01	1.6509552E-00 1.8977718E-00 1.8977718E-00 9.0196343E-00 7.6566829E-01 3.0831773E-01 -2.7402550E-01 -3.2904058E-02	2.1577250E-01 -3.9140298E-01 -3.9140298E-01 2.6091280E-01 1.8494025E-00 5.4900165E-01 -1.0230582E-00 -2.7007743E-00	5.0476596E-01 -4.5342523E-01 -4.5342523E-01 9.1257309E-01 8.3557484E-00 3.2278758E-00 -4.2434905E-00 -2.7981891E-01	1.8061893E-01 -3.2763575E-01 -3.2763575E-01 2.1840498E-01 1.5480985E-00 4.5955850E-01 -8.5688416E-01 -2.2607651E-00

















{ 1, 1, -11, 0 }	COS (-10L +12L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-1.4541197E-01	-1.6678072E 00	-1.9329053E 01	2.8138240E-02	3.2273244E-01	-5.4449478E-03
{ 3, 1, 0 }	5.4839258E 00	6.2246032E 01	7.1123015E 02	-1.0611783E 00	-1.2044659E 01	2.0534548E-01
{ 1, 3, 0 }	6.8949142E 00	7.8346289E 01	8.9661006E 02	-1.3342145E 00	-1.5160559E 01	2.5817991E-01
{ 1, 1, 1 }	3.4020124E 00	4.4580964E 01	6.0286883E 02	-6.5831338E-01	-8.6267309E 00	1.2738828E-01
{ 1, 1, -10, 0 }	COS (-9L +11L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-2.3187772E-01	-2.4287258E 00	-2.5761913E 01	5.0734042E-02	5.3139679E-01	-1.1100433E-02
{ 3, 1, 0 }	7.0781257E 00	7.3161681E 01	7.6184195E 02	-1.5486694E 00	-1.6007523E 01	3.3884350E-01
{ 1, 3, 0 }	9.1150801E 00	9.4365648E 01	9.8488173E 02	-1.9943480E 00	-2.0646877E 01	4.3635643E-01
{ 1, 1, 1 }	5.0028669E 00	6.0741219E 01	7.6548027E 02	-1.0946100E 00	-1.3289969E 01	2.3949687E-01
{ 1, 1, -9, 0 }	COS (-8L +10L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-3.0449996E-01	-3.4553996E 00	-3.3272047E 01	9.1740985E-02	8.6968942E-01	-2.3090286E-02
{ 3, 1, 0 }	8.7797222E 00	8.1801035E 01	7.6823930E 02	-2.2097681E 00	-2.0588500E 01	5.5617645E-01
{ 1, 3, 0 }	1.1646642E 01	1.0867636E 02	1.0251129E 03	-2.9313431E 00	-2.7375906E 01	7.3778966E-01
{ 1, 1, 1 }	7.2029501E 00	8.0574077E 01	9.4260156E 02	-1.8129103E 00	-2.0279687E 01	4.5629134E-01
{ 1, 1, -8, 0 }	COS (-7L +9L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-5.6297753E-01	-4.7779490E 00	-4.1360934E 01	1.6676725E-01	1.415315E 00	-4.9400402E-02
{ 3, 1, 0 }	1.0357777E 01	8.5857652E 01	7.1735536E 02	-3.062184E 00	-2.5433066E 01	9.0857852E-01
{ 1, 3, 0 }	1.6261903E 01	1.1870961E 02	9.9765294E 02	-4.2264902E 00	-3.5164593E 01	1.2519863E 00
{ 1, 1, 1 }	1.0108322E 01	1.0353031E 02	1.1199476E 03	-2.9943239E 00	-3.0668126E 01	8.8698951E-01
{ 1, 1, -7, 0 }	COS (-6L +8L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-8.3047572E-01	-6.3752097E 00	-4.9042420E 01	3.0609018E-01	2.2944677E 00	-1.1016328E-01
{ 3, 1, 0 }	1.1446141E 01	8.2934541E 01	6.0463678E 02	-4.1195197E 00	-2.9851767E 01	1.4826343E 00
{ 1, 3, 0 }	1.6569006E 01	1.2083350E 02	8.9026171E 02	-5.9635866E 00	-4.3488538E 01	2.1463226E 00
{ 1, 1, 1 }	1.3744320E 01	1.2800282E 02	1.2759351E 03	-4.9466450E 00	-4.6068812E 01	1.7803206E 00
{ 1, 1, -6, 0 }	COS (-5L +7L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-1.2483869E 00	-8.1247830E 00	-5.4773367E 01	5.7233963E-01	3.7249153E 00	-2.6239675E-01
{ 3, 1, 0 }	1.15684635E 01	7.1440163E 01	4.4008465E 02	-5.3041750E 00	-3.2752497E 01	2.4317699E 00
{ 1, 3, 0 }	1.7939129E 01	1.1210560E 02	7.0609818E 02	-8.2244335E 00	-5.1396311E 01	3.7706014E 00
{ 1, 1, 1 }	1.7956726E 01	1.5095281E 02	1.3832222E 03	-8.2325008E 00	-6.9206334E 01	3.7742999E 00
{ 1, 1, -5, 0 }	COS (-4L +6L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-1.7627464E 00	-9.7396545E 00	-5.6601876E 01	1.1129256E 00	6.1492174E 00	-7.0265547E-01
{ 3, 1, 0 }	1.0267074E 01	5.1738048E 01	2.5146301E 02	-6.4822088E 00	-3.2665276E 01	4.0926001E 00
{ 1, 3, 0 }	1.7631426E 01	9.1254952E 01	4.7018836E 02	-1.1131757E 01	-5.7614625E 01	7.0281341E 00
{ 1, 1, 1 }	2.2272671E 01	1.6780519E 02	1.4137193E 03	-1.4062049E 01	-1.0594530E 02	8.8781995E 00
{ 1, 1, -4, 0 }	COS (-3L +5L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-2.35536230E 00	-1.0718385E 01	-5.2721683E 01	2.3873224E 00	1.0864282E 01	-2.4198181E 00
{ 3, 1, 0 }	7.3668380E 00	2.7415279E 01	7.9995395E 01	-7.4671139E 00	-2.7788450E 01	7.5687546E 00
{ 1, 3, 0 }	1.5019615E 01	6.0558486E 01	2.2902586E 02	-1.5224059E 01	-6.1382795E 01	1.5431286E 01
{ 1, 1, 1 }	2.5755861E 01	1.7303466E 02	1.3476070E 03	-2.6106444E 01	-1.7538997E 02	2.6461800E 01
{ 1, 1, -3, 0 }	COS (-2L +4L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-2.8903672E 00	-1.0385821E 01	-4.2603066E 01	7.4253480E 00	2.6681154E 01	-1.9075705E 01
{ 3, 1, 0 }	3.3933721E 00	5.2583752E 00	-3.4775064E 01	-8.7175666E 00	-1.3508756E 01	2.2395412E 01
{ 1, 3, 0 }	1.0077787E 01	2.6977014E 01	3.7550520E 01	-2.5889816E 01	-6.9303899E 01	6.6510888E 01
{ 1, 1, 1 }	2.6975582E 01	1.6195466E 02	1.1844769E 03	-6.9300219E 01	-4.1606120E 02	1.7803213E 02
{ 1, 1, -2, 0 }	COS (-1L +3L -1W -1W )	1 2 1 2	<sup>2</sup>	C/N	DC/N	C/N=N
{ 1, 1, 0 }	-3.0583461E 00	-8.1873055E 00	-2.0417309E 01	-1.4699530E 01	-3.9351187E 01	-7.0651324E 01
{ 3, 1, 0 }	-1.4432226E-01	-7.4379624E 00	-7.1191986E 01	-6.9366561E-01	-3.5749570E 01	-3.3340108E 00
{ 1, 3, 0 }	4.0031281E 00	7.4838786E-01	-6.6777523E 01	1.9240499E 01	3.5970260E 00	9.2476879E 01
{ 1, 1, 1 }	2.4371230E 01	1.3385761E 02	9.5050274E 02	1.1713705E 02	6.4336867E 02	5.6300355E 02







( 0, 2, 6, 0 )	COS ( +6L -4L +0W -2W )	1 2 1 2				
			C	DC	D C	C/N
0 0, 2, 0, 0 )	2.5370464E-02	1.5701429E-01	9.9252933E-01	5.7801275E-03	3.5772410E-02	1.3168807E-03
0 2, 2, 0, 0 )	-6.2595080E-01	-3.7690972E-00	-2.2386210E-01	-1.4260975E-01	-0.5870966E-01	-3.2490636E-02
0 0, 4, 0, 0 )	-8.8666059E-02	-4.9845531E-01	-2.4503961E-00	-2.0200700E-02	-1.1356258E-01	-4.6023052E-03
0 0, 2, 1, 1 )	-2.3620691E-01	-1.8811549E-00	-1.7648928E-01	-5.3814785E-02	-4.2858164E-01	-1.2260569E-02
t 0, 2, 7, 0 )	COS ( +7L -5L +0W -2W )	1 2 1 2			2	
			C	DC	D C	C/N
0 0, 2, 0, 0 )	2.0144569E-02	1.4438954E-01	1.0462289E-00	4.0397637E-03	2.8955678E-02	8.1012858E-04
0 2, 2, 0, 0 )	-6.8942924E-01	-4.8824249E-00	-3.4572053E-01	-1.3825718E-01	-9.7911468E-01	-2.7725902E-02
0 0, 4, 0, 0 )	-1.1944622E-01	-8.3221906E-01	-5.6796002E-00	-2.3953578E-02	-1.6689205E-01	-4.8036172E-03
0 0, 2, 1, 1 )	-2.0353463E-01	-1.6955636E-00	-1.5507441E-01	-4.0816550E-02	-3.4002595E-01	-8.1852942E-03
0 0, 2, 8, 0 )	COS ( +8L -6L +0W -2W )	1 2 1 2			2	
			C	DC	D C	C/N
0 0, 2, 0, 0 )	1.4940920E-02	1.2209661E-01	1.0049248E-00	2.6757211E-03	2.1865887E-02	4.7918627E-04
0 2, 2, 0, 0 )	-6.7446350E-01	-5.4727383E-00	-4.4527422E-01	-1.2078749E-01	-9.8009505E-01	-2.1631443E-02
0 0, 4, 0, 0 )	-1.3118313E-01	-1.0591473E-00	-8.5279939E-00	-2.3493164E-02	-1.8967928E-01	-4.2073150E-03
0 0, 2, 1, 1 )	-1.7080250E-01	-1.5515953E-00	-1.4835883E-01	-3.0508484E-02	-2.7787020E-01	-5.4779930E-03
0 0, 2, 9, 0 )	COS ( +9L -7L +0W -2W )	1 2 1 2			2	
			C	DC	D C	C/N
0 0, 2, 0, 0 )	1.0556413E-02	9.6954745E-02	8.9538878E-01	1.7078584E-03	1.5685426E-02	2.7629887E-04
0 2, 2, 0, 0 )	-6.0699980E-01	-5.5665124E-00	-5.0847701E-01	-9.8200972E-02	-8.9731975E-01	-1.5887042E-02
0 0, 4, 0, 0 )	-1.2765029E-01	-1.1643545E-00	-1.0636943E-01	-2.0651378E-02	-1.8837032E-01	-3.3409995E-03
0 0, 2, 1, 1 )	-1.3725785E-01	-1.3739536E-00	-1.4188429E-01	-2.2205698E-02	-2.2227944E-01	-3.5924570E-03
0 0, 2, 10, 0 )	COS ( +10L -8L +0W -2W )	1 2 1 2			2	
			C	DC	D C	C/N
0 0, 2, 0, 0 )	7.1958297E-03	7.3387322E-02	7.5192825E-01	1.0615645E-03	1.0826643E-02	1.5660727E-04
0 2, 2, 0, 0 )	-5.1325408E-01	-5.2130799E-00	-5.3121543E-01	-7.5717791E-02	-7.6905943E-01	-1.1170265E-02
0 0, 4, 0, 0 )	-1.1429784E-01	-1.1600991E-00	-1.1805956E-01	-1.6861784E-02	-1.7114358E-01	-2.4875342E-03
0 0, 2, 1, 1 )	-1.0573260E-01	-1.1638776E-00	-1.3092221E-01	-1.5598199E-02	-1.7170101E-01	-2.3011237E-03
t-1, 1, -10, 0 )	COS ( -11L +11L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	7.2890264E-02	7.5102327E-01	7.7921373E-00	-1.1093638E-02	-1.1430306E-01	1.6884122E-03
t-1, 1, -9, 0 )	COS ( +10L +10L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	1.1380450E-01	1.0571188E-00	9.8970066E-00	-1.9052703E-02	-1.7697868E-01	3.1897288E-03
t-1, 1, -8, 0 )	COS ( -9L +9L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	1.7427431E-01	1.4413024E-00	1.2025411E-01	-3.2418135E-02	-2.6810799E-01	6.0303522E-03
t-1, 1, -7, 0 )	COS ( -8L +8L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	2.0035515E-01	1.8864781E-00	1.3799822E-01	-5.4484549E-02	-3.9478346E-01	1.1401987E-02
t-1, 1, -6, 0 )	COS ( -7L +7L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	3.7644767E-01	2.3384874E-00	1.4661677E-01	-9.0033416E-02	-5.5928627E-01	2.1532916E-02
t-1, 1, -5, 0 )	COS ( -6L +6L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	5.2021945E-01	2.6856150E-00	1.3938718E-01	-1.4515517E-01	-7.4935855E-01	4.0502180E-02
t-1, 1, -4, 0 )	COS ( -5L +5L +1W -1W )	1 2 1 2			2	
			C	DC	D C	C/N
t 1, 1, 0, 0 )	6.7231866E-01	2.7451695E-00	1.1064043E-01	-2.2511390E-01	-9.1917101E-01	7.5375372E-02

$\theta_{-1, 1, -3, 0}$	$\cos(-4L_1 + 4L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$7.7843910E-01$	$2.2857480E\ 00$	$5.9973701E\ 00$	$-3.2580805E-01$	$-9.5667740E-01$	$1.3636376E-01$
$\theta_{-1, 1, -2, 0}$	$\cos(-3L_1 + 3L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$7.2534907E-01$	$1.1446824E\ 00$	$-2.4681659E-01$	$-4.0478365E-01$	$-6.3879412E-01$	$2.2589097E-01$
$\theta_{-1, 1, -1, 0}$	$\cos(-2L_1 + 2L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$-2.0874305E-01$	$-1.0190370E\ 00$	$-6.0144583E\ 00$	$1.7473471E-01$	$8.5301590E-01$	$-1.4626700E-01$
$\theta_{-1, 1, -6, 0}$	$\cos(-1L_1 + 1L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$-4.3460676E-01$	$-1.5688525E\ 00$	$-7.6761151E\ 00$	$7.2760159E-01$	$2.6265112E\ 00$	$-1.2181220E\ 00$
$\theta_{-1, 1, 1, 0}$	$\cos(+OL_1 + OL_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$-2.8412479E-01$	$-1.2827237E\ 00$	$-7.0303438E\ 00$			
$\theta_{3, 1, 0}$	$-7.1941382E-01$	$-5.0881553E\ 00$	$-4.3535353E\ 01$			
$\theta_{1, 3, 0}$	$-1.4312069E\ 00$	$-8.9278533E\ 00$	$-6.9166499E\ 01$			
$\theta_{5, 1, 0}$	$-9.3374614E-01$	$-1.0559312E\ 01$	$-1.3619998E\ 02$			
$\theta_{3, 3, 0}$	$-7.5298308E\ 00$	$-7.2669211E\ 01$	$-8.2140357E\ 02$			
$\theta_{1, 5, 0}$	$-6.2017982E\ 00$	$-5.1742496E\ 01$	$-5.2522450E\ 02$			
$\theta_{1, 1, 1}$	$9.0364333E\ 00$	$5.3498586E\ 01$	$4.3673134E\ 02$			
$\theta_{3, 1, 1}$	$6.7904094E\ 01$	$4.7901852E\ 02$	$5.5594799E\ 03$			
$\theta_{1, 3, 1}$	$7.6662566E\ 01$	$7.1075884E\ 02$	$7.8031026E\ 03$			
$\theta_{1, 1, 2}$	$-1.1660104E\ 02$	$-1.1365995E\ 03$	$-1.2927611E\ 04$			
$\theta_{-1, 1, 2, 0}$	$\cos(+1L_1 - 1L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$2.0991315E-01$	$-6.1333088E-02$	$-3.5487270E\ 00$	$3.5126095E-01$	$-1.0268145E-01$	$5.8806729E-01$
$\theta_{-1, 1, 3, 0}$	$\cos(+2L_1 - 2L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$4.2425114E-01$	$1.0962574E\ 00$	$1.6522353E\ 00$	$3.5513230E-01$	$9.1765559E-01$	$2.9727428E-01$
$\theta_{-1, 1, 4, 0}$	$\cos(+3L_1 - 3L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$4.4507666E-01$	$1.7555657E\ 00$	$6.5069223E\ 00$	$2.4882308E-01$	$9.7969974E-01$	$1.3885661E-01$
$\theta_{-1, 1, 5, 0}$	$\cos(+4L_1 - 4L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$3.6083051E-01$	$1.9359276E\ 00$	$9.7600104E\ 00$	$1.5939287E-01$	$8.1026350E-01$	$6.6712323E-02$
$\theta_{-1, 1, 6, 0}$	$\cos(+5L_1 - 5L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$2.9262567E-01$	$1.8033388E\ 00$	$1.1155339E\ 01$	$9.7980484E-02$	$6.0381581E-01$	$3.2807016E-02$
$\theta_{-1, 1, 7, 0}$	$\cos(+6L_1 - 6L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$2.1073991E-01$	$1.5198760E\ 00$	$1.1037166E\ 01$	$5.8802081E-02$	$4.2408612E-01$	$1.6407356E-02$
$\theta_{-1, 1, 8, 0}$	$\cos(+7L_1 - 7L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$1.4524007E-01$	$1.1976326E\ 00$	$9.9485461E\ 00$	$3.4736462E-02$	$2.8643279E-01$	$8.3077744E-03$
$\theta_{-1, 1, 9, 0}$	$\cos(+8L_1 - 8L_2 + 1W_1 - 1W_2)$	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{2}{2}$	$\frac{2}{DC} \frac{DC}{DC}$	$C/N$	$DC/N$	$C/N/N$
$\theta_{1, 1, 0}$	$9.6960071E-02$	$8.9885844E-01$	$8.3914344E\ 00$	$2.0290844E-02$	$1.8810419E-01$	$4.2462668E-03$

$\ell = 1, 1, 10, 0$	$\cos(\ell + 9L - 9L + 1W - 1W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ \ell, 1, 1, 0 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 6.3183604E-02 & 6.5009517E-01 & 6.7318786E 00 \\ 1.1753279E-02 & 1.2092931E-01 & 2.1863198E-03 \end{matrix}$
$\ell = 0, 0, -7, 1$	$\cos(\ell - 6L + 8L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 4.3413610E-02 & 4.0693702E-01 & 3.988605E 00 \\ -1.9252317E 01 & 1.6715434E-01 & 1.4645853E-01 \\ 6.2219307E-01 & -3.3938118E 00 & -1.0159626E-02 \\ -1.6800217E 00 & -1.4733618E 01 & 5.3026977E 00 \\ -7.2656778E-01 & -8.1625395E 00 & -2.1761550E-01 \end{matrix}$
$\ell = 0, 0, -6, 1$	$\cos(\ell - 5L + 7L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 7.4672676E-02 & 6.2626941E-01 & 5.5522260E 00 \\ -3.4234686E-02 & -2.8712157E-01 & 1.5695349E-02 \\ -3.2219307E-01 & -1.0686158E 00 & -6.7721326E-02 \\ -2.1143373E 00 & -1.61117281E 01 & 7.3891630E 00 \\ -1.1136446E 00 & -1.1493813E 01 & -2.3407544E-01 \end{matrix}$
$\ell = 0, 0, -5, 1$	$\cos(\ell - 4L + 6L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 1.2723560E-01 & 9.4208562E-01 & 7.4931989E 00 \\ 7.3051466E-02 & 3.0768530E 00 & -5.9479413E-01 \\ -2.4716606E 00 & -1.5764860E 01 & 2.9119340E-02 \\ -1.6666411E 00 & -1.5721527E 01 & -9.8523862E-01 \end{matrix}$
$\ell = 0, 0, -4, 1$	$\cos(\ell - 3L + 5L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 2.1404162E-01 & 1.3759568E 00 & -8.0331329E-02 \\ 8.5016803E-01 & 9.3746370E 00 & -5.9426524E-01 \\ -2.5748180E 00 & -1.2640872E 01 & 1.9425985E 00 \\ -2.4179271E 00 & -2.0755257E 01 & -9.5528434E 00 \end{matrix}$
$\ell = 0, 0, -3, 1$	$\cos(\ell - 2L + 4L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 3.5367759E-01 & 1.9316894E 00 & -2.1697538E-01 \\ 2.0807919E 00 & 1.7255655E 01 & -1.3946861E 00 \\ -2.1633392E 00 & -5.9246175E 00 & 2.1992881E-01 \\ -3.3630519E 00 & -2.6227023E 01 & 8.7347014E-01 \end{matrix}$
$\ell = 0, 0, -2, 1$	$\cos(\ell - 1L + 3L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 5.6824795E-01 & 2.5654474E 00 & -9.0859706E-01 \\ 3.5921294E 00 & 2.4825208E 01 & -4.9625065E 00 \\ -9.5386733E-01 & 4.3016289E 00 & 2.3341842E 00 \\ -4.4106728E 00 & -3.1389979E 01 & 8.2982335E 01 \end{matrix}$
$\ell = 0, 0, -1, 1$	$\cos(\ell + 0L + 2L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 8.6921352E-01 & 3.1377049E 00 & 1.0792701E 00 \\ 4.6224838E 00 & 2.8723126E 01 & 3.8959717E 00 \\ 1.456297E 00 & 1.6172306E 01 & 1.3400896E 00 \\ -5.2940982E 00 & -3.5159796E 01 & 7.1266065E 00 \end{matrix}$
$\ell = 0, 0, -0, 1$	$\cos(\ell + 1L + 1L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 6.4363134E-01 & 2.8291341E 00 & 4.5885638E-01 \\ 3.8385634E 00 & 2.5976088E 01 & 2.0169407E 00 \\ 3.8385634E 00 & 2.5976088E 01 & 3.2712699E-01 \\ -5.5471720E 00 & -3.6520874E 01 & 1.9509580E 00 \end{matrix}$
$\ell = 0, 0, 1, 1$	$\cos(\ell + 2L + 0L + 0W + 0W)$	$\begin{matrix} & & 2 \\ \text{C} & \text{DC} & \text{D C} \\ 0, 0, 0, 1 \end{matrix}$	$\begin{matrix} & & 2 \\ \text{C/N} & \text{DC/N} & \text{C/N+N} \\ 8.6921352E-01 & 3.1377049E 00 & 4.3460676E-01 \\ 1.1456297E 00 & 1.6172306E 01 & 1.5688525E 00 \\ 4.6224838E 00 & 2.8723126E 01 & 2.1730338E-01 \\ -5.2940982E 00 & -3.5159796E 01 & 2.0664074E-01 \end{matrix}$



$\ell = 3, m = -3, \alpha = 0$	$\cos(\ell + 0L_1 + 3L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-1.3873945E-01}$	$\frac{DC/N}{-5.5597737E-01}$	$\frac{DC/N}{-2.2851451E-00}$	$\frac{C/N=N}{-4.6022431E-01}$
$\ell = 3, m = -2, \alpha = 0$	$\cos(\ell + 1L_1 + 2L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-5.3053958E-00}$	$\frac{DC/N}{-1.0557910E-01}$	$\frac{DC/N}{-4.8009881E-01}$	$\frac{C/N=N}{-5.8480535E-02}$
$\ell = 3, m = -1, \alpha = 0$	$\cos(\ell + 2L_1 + 1L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-7.0298451E-03}$	$\frac{DC/N}{-7.4751098E-02}$	$\frac{DC/N}{-2.9258279E-03}$	
$\ell = 3, m = -0, \alpha = 0$	$\cos(\ell + 3L_1 + 0L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-5.6025634E-03}$	$\frac{DC/N}{-2.0640711E-02}$	$\frac{DC/N}{-1.8675211E-03}$	
$\ell = 3, m = 1, \alpha = 0$	$\cos(\ell + 4L_1 - 1L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-4.6631679E-03}$	$\frac{DC/N}{-1.5231155E-02}$	$\frac{DC/N}{-1.2962915E-03}$	
$\ell = 3, m = 2, \alpha = 0$	$\cos(\ell + 5L_1 - 2L_2 - 3W_1 + 0W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{5.3038141E-02}$	$\frac{DC/N}{1.0081677E-01}$	$\frac{DC/N}{1.2644300E-02}$	
$\ell = 2, m = -12, \alpha = 0$	$\cos(\ell - 9L_1 + 12L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{1.5015527E-02}$	$\frac{DC/N}{-2.6863753E-01}$	$\frac{DC/N}{-3.0930423E-00}$	$\frac{C/N=N}{6.4455932E-02}$
$\ell = 2, m = -10, \alpha = 0$	$\cos(\ell - 8L_1 + 11L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{1.8104823E-02}$	$\frac{DC/N}{-4.5140163E-01}$	$\frac{DC/N}{-4.7504566E-00}$	$\frac{C/N=N}{1.2642688E-01}$
$\ell = 2, m = -8, \alpha = 0$	$\cos(\ell - 7L_1 + 10L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{2.0926559E-02}$	$\frac{DC/N}{-7.6034672E-01}$	$\frac{DC/N}{-7.2508453E-00}$	$\frac{C/N=N}{2.5573845E-01}$
$\ell = 2, m = -6, \alpha = 0$	$\cos(\ell - 6L_1 + 9L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{2.2974921E-02}$	$\frac{DC/N}{-1.2922832E-00}$	$\frac{DC/N}{-1.1051841E-01}$	$\frac{C/N=N}{5.4392967E-01}$
$\ell = 2, m = -4, \alpha = 0$	$\cos(\ell - 5L_1 + 8L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{2.3663072E-02}$	$\frac{DC/N}{-2.2502148E-00}$	$\frac{DC/N}{-1.7041639E-01}$	$\frac{C/N=N}{1.2652221E-00}$
$\ell = 2, m = -2, \alpha = 0$	$\cos(\ell - 4L_1 + 7L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{2.2474871E-02}$	$\frac{DC/N}{-4.1835598E-00}$	$\frac{DC/N}{-2.7622926E-01}$	$\frac{C/N=N}{3.5417896E-00}$
$\ell = 2, m = -5, \alpha = 0$	$\cos(\ell - 3L_1 + 6L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{1.9213543E-02}$	$\frac{DC/N}{-9.6978055E-00}$	$\frac{DC/N}{-5.4756300E-01}$	$\frac{C/N=N}{1.4609096E-01}$
$\ell = 2, m = -4, \alpha = 0$	$\cos(\ell - 2L_1 + 5L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{1.4284050E-02}$	$\frac{DC/N}{4.3286185E-02}$	$\frac{DC/N}{2.0418414E-03}$	$\frac{C/N=N}{3.2233380E-04}$
$\ell = 4, m = 1, \alpha = 0$	$\cos(\ell - 6L_1 + 25L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{3.3703052E-01}$	$\frac{DC/N}{-4.6388624E-02}$	$\frac{DC/N}{-1.2511146E-03}$	$\frac{C/N=N}{-3.4543634E-04}$
$\ell = 2, m = 3, \alpha = 0$	$\cos(\ell - 5L_1 + 18L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{-4.5933919E-02}$	$\frac{DC/N}{-2.6181011E-03}$	$\frac{DC/N}{-1.0277729E-04}$	$\frac{C/N=N}{-1.9495885E-05}$
$\ell = 6, m = 1, \alpha = 0$	$\cos(\ell - 7L_1 + 23L_2 - 2W_1 - 1W_2)$	$\frac{C}{1} \quad \frac{DC}{2}$	$\frac{D}{2} \frac{C}{1}$	$\frac{C/N}{3.3126281E-02}$	$\frac{DC/N}{2.7896585E-02}$	$\frac{DC/N}{2.0206123E-03}$	$\frac{C/N=N}{2.0773400E-04}$

$\ell_{4, 3, 0}$	6.5242879E 01	3.7432573E 02	3.2163206E 03	4.8583596E 03	2.787444E 04	3.6178136E 05
$\ell_{2, 5, 0}$	8.6768304E 01	4.7123523E 02	3.5230227E 03	6.4612665E 03	3.5090882E 04	4.8114301E 05
$\ell_{2, 1, 1}$	-7.7253990E 01	-5.6454695E 02	-4.8220797E 03	-5.7527759E 03	-4.2039409E 04	-4.2838474E 05
$\ell_{4, 1, 1}$	-1.1657425E 02	-1.7655485E 03	-2.5555367E 04	-8.6807808E 03	-1.3147288E 05	-6.4642134E 05
$\ell_{2, 3, 1}$	3.4623326E 01	-1.5914745E 03	-3.4081271E 04	2.5931449E 03	-1.1851033E 05	1.9310047E 05
$\ell_{2, 1, 2}$	1.0222653E 03	1.0799970E 04	1.2980836E 05	7.6123748E 04	8.0422784E 05	5.6686115E 06
$\ell_{2, 1, -3, 0}$	$\cos(-\ell_1 + 4\ell_2 - 2\ell_3 - \ell_4)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	4.9935310E 00	1.9232105E 01	8.8195820E 01	8.1761550E 00	3.1489676E 01	1.3387222E 01
$\ell_{2, 1, -2, 0}$	$\cos(\ell_1 + 4\ell_2 + 3\ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	3.0478939E 00	9.7344029E 00	4.3412304E 01	2.5229711E 00	8.0578977E 00	2.0684530E 00
$\ell_{2, 1, -1, 0}$	$\cos(\ell_1 + \ell_2 + 2\ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	5.6438901E-01	2.8349661E 00	1.7695933E 01	3.1261654E-01	1.5702951E 00	1.7315911E-01
$\ell_{2, 1, -0, 0}$	$\cos(\ell_1 + 2\ell_2 + \ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	8.6258044E-02	7.4238943E-01	6.6854479E 00	2.7576650E-02	3.0898315E-01	1.1477430E-02
$\ell_{2, 1, 1, 0}$	$\cos(\ell_1 + 3\ell_2 + \ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	-8.3530004E-04	1.5569350E-01	2.1940005E 00	-2.7843335E-04	5.1897832E-02	-9.2011116E-05
$\ell_{2, 1, -2, 0}$	$\cos(\ell_1 + 4\ell_2 - \ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	-1.1320919E-01	-1.9243294E-01	2.0788766E-01	-3.1470476E-02	-5.3493503E-02	-8.7463257E-03
$\ell_{2, 1, 3, 0}$	$\cos(\ell_1 + 5\ell_2 - 2\ell_3 - 2\ell_4 - \ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{2, 1, 0}$	-1.9084008E-01	-5.6625502E-01	-1.5402971E 00	-4.5496301E-02	-1.3499528E-01	-1.0846325E-02
$\ell_{1, 2, -10, 0}$	$\cos(\ell_1 - 9\ell_2 + 12\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-1.9800064E 00	-2.0820406E 01	-2.2200359E 02	4.7507569E-01	4.9955743E 00	-1.1398797E-01
$\ell_{1, 2, -9, 0}$	$\cos(\ell_1 - 8\ell_2 + 11\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-2.8397585E 00	-2.7050560E 01	-2.6218964E 02	7.9534890E-01	7.5762219E 00	-2.2275834E-01
$\ell_{1, 2, -8, 0}$	$\cos(\ell_1 - 7\ell_2 + 10\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-3.9651113E 00	-3.3856505E 01	-2.9558736E 02	1.3336434E 00	1.1387450E 01	-4.4856364E-01
$\ell_{1, 2, -7, 0}$	$\cos(\ell_1 - 6\ell_2 + 9\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-5.3546172E 00	-4.0455606E 01	-3.1477234E 02	2.2537901E 00	1.7028004E 01	-9.4863360E-01
$\ell_{1, 2, -6, 0}$	$\cos(\ell_1 - 5\ell_2 + 8\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-6.9284300E 00	-4.5572091E 01	-3.1214269E 02	3.8956294E 00	2.5623696E 01	-2.1903849E 00
$\ell_{1, 2, -5, 0}$	$\cos(\ell_1 - 4\ell_2 + 7\ell_3 - \ell_4 - 2\ell_5)$					
	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N_{\text{N}}$
$\ell_{1, 2, 0}$	-8.4705524E 00	-4.7509485E 01	-2.8263198E 02	7.1711453E 00	4.0221393E 01	-6.0710708E 00

6 1, 2, -4, 0 )	COS ( -3L +6L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-9.5703142E 00	DC	D C	C/N	DC/N	C/N=N	
			-2.2741505E 02	1.6390746E 01	7.6309443E 01	-2.8071864E 01	
6 1, 2, -3, 0 )	COS ( -2L +5L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-9.6152096E 00	DC	D C	C/N	DC/N	C/N=N	
8 3, 2, 0 )	9.5215365E 00	DC	D C	C/N	DC/N	C/N=N	
8 1, 4, 0 )	3.0321975E 01	DC	D C	C/N	DC/N	C/N=N	
8 5, 2, 0 )	-9.5503238E 00	DC	D C	C/N	DC/N	C/N=N	
8 3, 4, 0 )	-7.5665532E 01	DC	D C	C/N	DC/N	C/N=N	
8 1, 6, 0 )	-5.2562976E 01	DC	D C	C/N	DC/N	C/N=N	
8 1, 2, 1 )	1.0630850E 02	DC	D C	C/N	DC/N	C/N=N	
8 3, 2, 1 )	3.3630404E 02	DC	D C	C/N	DC/N	C/N=N	
8 1, 4, 1 )	8.6189662E 01	DC	D C	C/N	DC/N	C/N=N	
8 1, 2, 2 )	-1.2800458E 03	DC	D C	C/N	DC/N	C/N=N	
		-1.2756219E 04	-1.4745685E 05	-9.5319566E 04	-9.4990132E 05	-7.0980424E 06	
6 1, 2, -2, 0 )	COS ( -1L +4L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-7.9592586E 00	DC	D C	C/N	DC/N	C/N=N	
		-2.2971065E 01	-8.9827712E 01	-1.3032087E 01	-3.7611659E 01	-2.1338080E 01	
6 1, 2, -1, 0 )	COS ( +0L +3L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-1.7303776E 00	DC	D C	C/N	DC/N	C/N=N	
		-7.5835449E 00	-4.0806516E 01	-1.4323637E 00	-6.2774706E 00	-1.1856752E 00	
6 1, 2, -0, 0 )	COS ( +1L +2L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-8.2681987E-01	DC	D C	C/N	DC/N	C/N=N	
		-3.4878812E 00	-2.0118649E 01	-4.5797766E-01	-1.9319464E 00	-2.5367501E-01	
6 1, 2, 1, 0 )	COS ( +2L +1L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-1.8567623E-01	DC	D C	C/N	DC/N	C/N=N	
		-1.1491594E 00	-8.5705233E 00	-7.7278613E-02	-4.7828118E-01	-3.2163428E-02	
6 1, 2, 2, 0 )	COS ( +3L +0L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	-4.0859269E-02	DC	D C	C/N	DC/N	C/N=N	
		-3.5324507E-01	-3.3595763E 00	-1.3619756E-02	-1.1774836E-01	-4.5399188E-03	
6 1, 2, 3, 0 )	COS ( +4L -1L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	1.0561248E-02	DC	D C	C/N	DC/N	C/N=N	
		-4.4718102E-02	-1.0511394E 00	2.9358702E-03	-1.2430969E-02	8.1612837E-04	
6 1, 2, 4, 0 )	COS ( +5L -2L -1W -2W )	$\frac{1}{1} \frac{2}{2} \frac{-1}{1} \frac{-2}{2}$					
8 1, 2, 0 )	4.7349206E-02	DC	D C	C/N	DC/N	C/N=N	
		1.6920106E-01	3.7592378E-01	1.1288057E-02	4.0337555E-02	2.6910745E-03	
6 0, 3,-10, 0 )	COS ( -10L +13L +0W -3W )	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{-3}{2}$					
8 0, 3, 0 )	7.9788868E-01	DC	D C	C/N	DC/N	C/N=N	
		8.3843396E 00	8.9319950E 01	-1.6744481E-01	-1.7595364E 00	3.5139944E-02	
6 0, 3,-9, 0 )	COS ( -9L +12L +0W -3W )	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{-3}{2}$					
8 0, 3, 0 )	1.1660175E 00	DC	D C	C/N	DC/N	C/N=N	
		1.1096843E 01	1.0742230E 02	-2.7977008E-01	-2.6625370E 00	6.7127038E-02	
6 0, 3,-8, 0 )	COS ( -8L +11L +0W -3W )	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{-3}{2}$					
8 0, 3, 0 )	1.6657826E 00	DC	D C	C/N	DC/N	C/N=N	
		1.4205106E 01	1.2379622E 02	-4.6654615E-01	-3.9785129E 00	1.3066850E-01	
6 0, 3,-7, 0 )	COS ( -7L +10L +0W -3W )	$\frac{1}{1} \frac{2}{2} \frac{1}{1} \frac{-3}{2}$					
8 0, 3, 0 )	2.3146589E 00	DC	D C	C/N	DC/N	C/N=N	
		1.7454585E 01	1.3544559E 02	-7.7852283E-01	-5.8708885E 00	2.6185188E-01	

$\ell_0, 3, -6, 0, 1 \quad \cos (-6L_1 + 9L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 3.1066125E\ 00 \quad 2.0374776E\ 01 \quad 1.3895798E\ 02 \quad -1.3075916E\ 00 \quad -8.5758638E\ 00 \quad 5.5037305E\ -01$

$\ell_0, 3, -5, 0, 1 \quad \cos (-5L_1 + 8L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 3.9873609E\ 00 \quad 2.2257517E\ 01 \quad 1.3144141E\ 02 \quad -2.2419626E\ 00 \quad -1.2514673E\ 01 \quad 1.2605822E\ 00$

$\ell_0, 3, -4, 0, 1 \quad \cos (-4L_1 + 7L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 4.0211547E\ 00 \quad 2.2251157E\ 01 \quad 1.1201700E\ 02 \quad -4.0815756E\ 00 \quad -1.8837765E\ 01 \quad 3.4554501E\ 00$

$\ell_0, 3, -3, 0, 1 \quad \cos (-3L_1 + 6L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 5.3597414E\ 00 \quad 1.9649199E\ 01 \quad 8.3440540E\ 01 \quad -9.1794437E\ 00 \quad -3.3652504E\ 01 \quad 1.5721316E\ 01$

$\ell_0, 3, -2, 0, 1 \quad \cos (-2L_1 + 5L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 5.2469687E\ 00 \quad 1.4442611E\ 01 \quad 5.2649406E\ 01 \quad 3.9071943E\ 02 \quad 1.0754798E\ 03 \quad 2.9095213E\ 04$   
 $\ell_0, 2, 3, 0, 1 \quad -4.2148704E\ 00 \quad 2.3651841E\ 01 \quad 3.4642027E\ 02 \quad -3.1386346E\ 02 \quad 1.7612520E\ 03 \quad -2.3372076E\ 04$   
 $\ell_0, 5, 0, 1 \quad -9.2122321E\ 00 \quad -1.2563707E\ 01 \quad 4.4871072E\ 01 \quad -6.8599573E\ 02 \quad -9.3556579E\ 02 \quad -5.1083183E\ 04$   
 $\ell_0, 4, 3, 0, 1 \quad 1.3355317E\ 01 \quad 1.2979491E\ 02 \quad 1.7338600E\ 03 \quad 9.4951364E\ 02 \quad 9.6652750E\ 03 \quad 7.4057199E\ 04$   
 $\ell_0, 2, 5, 0, 1 \quad 4.9252770E\ 01 \quad 2.9376791E\ 02 \quad 3.2125018E\ 03 \quad 3.3454309E\ 03 \quad 2.1875446E\ 04 \quad 2.4912000E\ 05$   
 $\ell_0, 7, 0, 1 \quad 1.33227794E\ 01 \quad 6.7707614E\ 01 \quad 6.0592969E\ 02 \quad 9.9209177E\ 02 \quad 5.0418980E\ 03 \quad 7.3876854E\ 04$   
 $\ell_0, 3, 1, 1 \quad -4.6104142E\ 01 \quad -2.6791869E\ 02 \quad -2.0174739E\ 03 \quad -3.4331793E\ 03 \quad -1.9950765E\ 04 \quad -2.5565425E\ 05$   
 $\ell_0, 2, 3, 1, 1 \quad -3.8693159E\ 02 \quad -4.1345559E\ 03 \quad -4.8973902E\ 04 \quad -2.8813149E\ 04 \quad -3.0788279E\ 05 \quad -2.1455926E\ 06$   
 $\ell_0, 5, 1, 1 \quad -6.9156293E\ 01 \quad -1.0243072E\ 03 \quad -1.2388700E\ 04 \quad -5.1497749E\ 03 \quad -7.6275797E\ 04 \quad -3.0366182E\ 05$   
 $\ell_0, 3, 2, 1 \quad 5.0743892E\ 02 \quad 4.8187953E\ 03 \quad 5.4070237E\ 04 \quad 3.7788617E\ 04 \quad 3.5883518E\ 05 \quad 2.8138234E\ 06$

$\# \ell_0, 3, -1, 0, 1 \quad \cos (-1L_1 + 4L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 1.2252813E\ 00 \quad 5.0765059E\ 00 \quad 2.5426754E\ 01 \quad 2.0062135E\ 00 \quad 8.3120139E\ 00 \quad 3.2846726E\ 00$

$\ell_0, 3, -0, 0, 1 \quad \cos (+0L_1 + 3L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 2.0038058E\ 00 \quad 3.0556562E\ 00 \quad 1.4713868E\ 01 \quad 1.6587008E\ 00 \quad 2.5293966E\ 00 \quad 1.3730315E\ 00$

$\# \ell_0, 3, 1, 0, 1 \quad \cos (+1L_1 + 2L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 2.4568864E\ -01 \quad 1.1965809E\ 00 \quad 7.2321799E\ 00 \quad 1.3608757E\ -01 \quad 6.6278926E\ -01 \quad 7.5379258E\ -02$

$\ell_0, 3, 2, 0, 1 \quad \cos (+2L_1 + 1L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 7.6587647E\ -02 \quad 4.6198099E\ -01 \quad 3.3519721E\ 00 \quad 3.1875848E\ -02 \quad 1.9227691E\ -01 \quad 1.3266757E\ -02$

$\ell_0, 3, 3, 0, 1 \quad \cos (+3L_1 + 0L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 2.1339948E\ -02 \quad 1.6593965E\ -01 \quad 1.4554569E\ 00 \quad 7.1133161E\ -03 \quad 5.5313215E\ -02 \quad 2.3711053E\ -03$

$\ell_0, 3, 4, 0, 1 \quad \cos (+4L_1 - 1L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad 5.3964314E\ -03 \quad 5.5581512E\ -02 \quad 5.9423830E\ -01 \quad 1.5001279E\ -03 \quad 1.5450836E\ -02 \quad 4.1701331E\ -04$

$\ell_0, 3, 5, 0, 1 \quad \cos (+5L_1 - 2L_2 + 0W_1 - 3W_2)$   
 C DC DC C/N DC/N C/N=N  
 $\ell_0, 3, 0, 1 \quad -2.0662960E\ -03 \quad 9.8924857E\ -04 \quad 1.4689695E\ -01 \quad -4.9260526E\ -04 \quad 2.3583700E\ -04 \quad -1.1743716E\ -04$

$(-1, 2, -1C, 0, 1) \quad \cos (-11L_1 + 12L_2 + 1W_1 - 2W_2)$   
 C DC DC C/N DC/N C/N=N  
 $(1, 2, 0, 1) \quad 6.1927209E\ -01 \quad 6.3942801E\ 00 \quad 6.6518945E\ 01 \quad -1.0040453E\ -01 \quad -1.0367247E\ 00 \quad 1.6278902E\ -02$

$t-1, 2, -9, 0)$   $\cos(-10L + 11L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 8.8114573E-01 & 8.2044603E 00 & 7.7040302E 01 & -1.5818197E-01 & -1.4728525E 00 & 2.8396592E-02 \end{array}$   
  
 $t-1, 2, -8, 0)$   $\cos(-9L + 10L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 1.2178923E 00 & 1.0098999E 01 & 8.4532732E 01 & -2.4489393E-01 & -2.0307080E 00 & 4.9243301E-02 \end{array}$   
  
 $t-1, 2, -7, 0)$   $\cos(-8L + 9L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 1.6227170E 00 & 1.1790996E 01 & 8.6532201E 01 & -3.7083658E-01 & -2.6945750E 00 & 8.4746611E-02 \end{array}$   
  
 $t-1, 2, -6, 0)$   $\cos(-7L + 8L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 2.0609928E 00 & 1.2837154E 01 & 8.0676571E 01 & -5.4545068E-01 & -3.3974083E 00 & 1.4435589E-01 \end{array}$   
  
 $t-1, 2, -5, 0)$   $\cos(-6L + 7L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 2.4519092E 00 & 1.2676947E 01 & 6.5693411E 01 & -7.7074993E-01 & -3.9849582E 00 & 2.4220281E-01 \end{array}$   
  
 $t-1, 2, -4, 0)$   $\cos(-5L + 6L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 2.6518776E 00 & 1.0791537E 01 & 4.2700292E 01 & -1.0263140E 00 & -4.1764771E 00 & 3.9719799E-01 \end{array}$   
  
 $t-1, 2, -3, 0)$   $\cos(-4L + 5L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 2.4590575E 00 & 7.0392249E 00 & 1.6203081E 01 & -1.2378402E 00 & -3.5434044E 00 & 6.2310392E-01 \end{array}$   
  
 $t-1, 2, -2, 0)$   $\cos(-3L + 4L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & 1.6833607E 00 & 2.1325262E 00 & -6.4735574E 00 & -1.2116988E 00 & -1.5350122E 00 & 8.7219206E-01 \end{array}$   
  
 $t-1, 2, -1, 0)$   $\cos(-2L + 3L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -5.6081614E-01 & -3.0011575E 00 & -1.9637112E 01 & 7.0815251E-01 & 3.7896149E 00 & -8.9419675E-01 \end{array}$   
  
 $t-1, 2, -0, 0)$   $\cos(-1L + 2L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -8.2681987E-01 & -3.4878812E 00 & -2.0118649E 01 & 4.2481974E 00 & 1.7920720E 01 & -2.1827222E 01 \end{array}$   
  
 $t-1, 2, 1, 0)$   $\cos(-OL + 1L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -4.8864645E-01 & -2.4978048E 00 & -1.5872452E 01 & -1.2134683E 00 & -6.2028628E 00 & -3.0134371E 00 \end{array}$   
  
 $t-1, 2, 2, 0)$   $\cos(+1L + 0L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -2.1959322E-01 & -1.3950550E 00 & -1.0352777E 01 & -2.1959322E-01 & -1.3950550E 00 & -2.1959322E-01 \end{array}$   
  
 $t-1, 2, 3, 0)$   $\cos(+2L - 1L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -1.4522486E-01 & -8.5269977E-01 & -6.4356467E 00 & -9.0918155E-02 & -5.3383346E-01 & -5.6919393E-02 \end{array}$   
  
 $t-1, 2, 4, 0)$   $\cos(+3L - 2L + 1W - 2W)$   
 $\begin{array}{ccccccc} & C & DC & \overset{2}{DC} & C/N & DC/N & C/N=N \\ t-1, 2, 0) & -1.8205647E-01 & -9.0845708E-01 & -5.5381244E 00 & -8.2955488E-02 & -4.1394573E-01 & -3.7799333E-02 \end{array}$





$\theta_{1,0,1,1}$	$\cos(-3L_1 + 0L_2 - 1W_1 + 0W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,0,1,1}$	$1.6957458E-01$	$-1.4007053E\ 00$	$-1.9065676E\ 01$	$5.6524861E-02$	$-4.6690175E-01$	$1.8841620E-02$
$\theta_{1,0,2,1}$	$\cos(+4L_1 - 1L_2 - 1W_1 + 0W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,0,2,1}$	$4.2202508E-01$	$6.5830789E-01$	$-5.5150708E\ 00$	$1.1731671E-01$	$1.8299983E-01$	$3.2612306E-02$
$\theta_{0,1,-6,1}$	$\cos(-5L_1 + 0L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$8.7317978E-01$	$7.4731336E\ 00$	$6.8005420E\ 01$	$-4.9096041E-01$	$-4.2018984E\ 00$	$2.7605097E-01$
$\theta_{0,1,-9,1}$	$\cos(-4L_1 + 7L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$1.2980742E\ 00$	$9.8701560E\ 00$	$8.1259639E\ 01$	$-1.0989459E\ 00$	$-8.3560455E\ 00$	$9.3036441E-01$
$\theta_{0,1,-4,1}$	$\cos(-3L_1 + 6L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$1.8653174E\ 00$	$1.2433229E\ 01$	$9.2171166E\ 01$	$-3.1946645E\ 00$	$-2.1293962E\ 01$	$5.4713914E\ 00$
$\theta_{0,1,-3,1}$	$\cos(-2L_1 + 5L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$2.5573939E\ 00$	$1.4717762E\ 01$	$9.8166105E\ 01$	$1.9043824E\ 02$	$1.0959691E\ 03$	$1.4181125E\ 04$
$\theta_{2,1,1,1}$	$1.7991391E\ 01$	$1.5896171E\ 02$	$1.6014554E\ 03$	$1.3397423E\ 03$	$1.1837202E\ 04$	$9.9764912E\ 04$
$\theta_{0,3,1,1}$	$-1.0171392E\ 01$	$-2.7977633E\ 01$	$1.0942175E\ 02$	$-7.5742027E\ 02$	$-2.0833753E\ 03$	$-5.6401864E\ 04$
$\theta_{0,1,2,1}$	$-2.8250845E\ 01$	$-2.3647855E\ 02$	$-2.2988840E\ 03$	$-2.1037202E\ 03$	$-1.7609551E\ 04$	$-1.5665509E\ 05$
$\theta_{0,1,-2,1}$	$\cos(-1L_1 + 4L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$3.2715973E\ 00$	$1.6017100E\ 01$	$9.7009516E\ 01$	$5.3567478E\ 00$	$2.6225589E\ 01$	$8.7708678E\ 00$
$\theta_{0,1,-1,1}$	$\cos(-40L_1 + 3L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$3.7416863E\ 00$	$1.5520377E\ 01$	$8.8150711E\ 01$	$3.0974408E\ 00$	$1.2847384E\ 01$	$2.5639840E\ 00$
$\theta_{0,1,-0,1}$	$\cos(+1L_1 + 2L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$2.3800140E\ 00$	$1.1793523E\ 01$	$7.2710089E\ 01$	$1.3182959E\ 00$	$6.5324631E\ 00$	$7.3020753E-01$
$\theta_{0,1,1,2}$	$\cos(+2L_1 + 1L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$2.0034592E\ 00$	$9.2449676E\ 00$	$5.7446252E\ 01$	$8.3384154E-01$	$3.8477639E\ 00$	$3.4704560E-01$
$\theta_{0,1,2,1}$	$\cos(+3L_1 + 0L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$9.9059890E-01$	$5.7553106E\ 00$	$4.0705242E\ 01$	$3.3286630E-01$	$1.9184369E\ 00$	$1.1095543E-01$
$\theta_{0,1,3,1}$	$\cos(+4L_1 - 1L_2 + 0W_1 - 1W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,1,1,1}$	$4.3532832E-01$	$3.1276257E\ 00$	$2.5864187E\ 01$	$1.2101482E-01$	$8.6943357E-01$	$3.3640324E-02$
$\theta_{-1,0,-6,1}$	$\cos(-6L_1 + 7L_2 + 1W_1 + 0W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,0,1,1}$	$4.0228682E-02$	$3.5523402E-01$	$1.3974045E\ 00$	$-1.8932696E-02$	$-1.1166669E-01$	$5.9514334E-03$
$\theta_{-1,0,-5,1}$	$\cos(-5L_1 + 6L_2 + 1W_1 + 0W_2)$	$1 \quad 2$	$2$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,0,1,1}$	$3.7899604E-02$	$2.1743053E-02$	$-2.5810509E\ 00$	$-1.4667681E-02$	$-8.4148681E-03$	$5.6765993E-03$

8-1, 0, -4, 1 )	COS ( -4L +5L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -4.8793540E-02 -7.3759640E-01 -9.4582287E 00 2.3051549E-02 3.7129124E-01 -1.1603688E-02					
8-1, 0, -3, 1 )	COS ( -3L +4L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -2.5848953E-01 -2.1617810E 00 -1.9839027E 01 1.8606317E-01 1.5560701E 00 -1.3393001E-01					
8-1, 0, -2, 1 )	COS ( -2L +3L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -7.1447410E-01 -4.4725869E 00 -3.3867208E 01 9.0217915E-01 5.6476150E 00 -1.1391976E 00					
8-1, 0, -1, 1 )	COS ( -1L +2L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -1.5688525E 00 -7.6761151E 00 -4.9770136E 01 8.0607580E 00 3.9439850E 01 -4.1416144E 01					
8-1, 0, -0, 1 )	COS ( +0L +1L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -2.0581984E 00 -1.0378956E 01 -6.5160286E 01 -5.1111770E 00 -2.5774329E 01 -1.2692717E 01					
8-1, 0, 1, 1 )	COS ( +1L +0L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -3.3072795E 00 -1.3951525E 01 -8.0474996E 01 -3.3072795E 00 -1.3951525E 01 -3.3072795E 00					
8-1, 0, 2, 1 )	COS ( +2L -1L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -2.9874725E 00 -1.4734376E 01 -8.9971462E 01 -1.8703098E 00 -9.2244698E 00 -1.1709092E 00					
8-1, 0, 3, 1 )	COS ( +3L -2L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -2.3805551E 00 -1.3751917E 01 -9.2140944E 01 -1.0847190E 00 -6.2661713E 00 -4.9426088E-01					
8-1, 0, 4, 1 )	COS ( +4L -3L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -1.7582866E 00 -1.1745251E 01 -8.7305698E 01 -6.2977174E-01 -4.2068383E 00 -2.2556758E-01					
8-1, 0, 5, 1 )	COS ( +5L -4L +1W +0W ) 1 2 1 2					
8 1, 0, 1 )	C DC D C -1.2344566E 00 -9.3991133E 00 -7.7513040E 01 -3.6422629E-01 -2.7732078E 00 -1.0746494E-01					
8 0,-1, -6, 1 )	COS ( -4L +5L +0W +1W ) 1 2 1 2					
8 0, 1, 1 )	C DC D C -2.2875301E-01 -1.4346715E 00 -8.6587476E 00 1.1514968E-01 7.2228553E-01 -5.7964038E-02					
8 0,-1, -4, 1 )	COS ( -3L +4L +0W +1W ) 1 2 1 2					
8 0, 1, 1 )	C DC D C -2.7529890E-01 -1.3263389E 00 -5.1381720E 00 1.9816271E-01 9.5471107E-01 -1.4263937E-01					
8 0,-1, -3, 1 )	COS ( -2L +3L +0W +1W ) 1 2 1 2					
8 0, 1, 1 )	C DC D C -2.7202686E-01 -7.3575310E-01 1.7635476E 00 3.4349315E-01 9.2904851E-01 -4.3373491E-01					
8 0,-1, -2, 1 )	COS ( -1L +2L +0W +1W ) 1 2 1 2					
8 0, 1, 1 )	C DC D C -1.3790028E-01 6.2441580E-01 1.2553105E 01 7.0853114E-01 -3.2082461E 00 -3.6404303E 00					

$\theta_{0,-1,-1,1}$	$\cos(-4\omega_1 + \omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$2.6503210E-01$	$2.9695577E-00$	$2.6741791E-01$	$6.5816122E-01$	$7.3743790E-00$	$1.6344287E-00$
$\theta_{0,-1,-0,1}$	$\cos(-\omega_1 + \omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.0927514E-00$	$6.1352553E-00$	$4.2510800E-01$	$1.0927514E-00$	$6.1352553E-00$	$1.0927514E-00$
$\theta_{0,-1,1,1}$	$\cos(\omega_1 - \omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$2.0034592E-00$	$9.2449676E-00$	$5.7446252E-01$	$1.2542675E-00$	$5.7878203E-00$	$7.8523527E-01$
$\theta_{0,-1,2,1}$	$\cos(-3\omega_1 - 2\omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$2.1350981E-00$	$1.0886205E-01$	$6.8857380E-01$	$9.7287453E-01$	$4.9603866E-00$	$4.4329807E-01$
$\theta_{0,-1,3,1}$	$\cos(-4\omega_1 - 3\omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.8500387E-00$	$1.0854383E-01$	$7.4065405E-01$	$6.6263493E-01$	$3.8877531E-00$	$2.3733830E-01$
$\theta_{0,-1,4,1}$	$\cos(-4\omega_1 - 4\omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.4371941E-00$	$9.6813158E-00$	$7.2709298E-01$	$4.2404402E-01$	$2.8564716E-00$	$1.2511416E-01$
$\theta_{0,-1,5,1}$	$\cos(-6\omega_1 - 5\omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.0436030E-00$	$7.9859848E-00$	$6.6273242E-01$	$2.6177962E-01$	$2.0032215E-00$	$6.3663359E-02$
$\theta_{0,-1,6,1}$	$\cos(-7\omega_1 - 6\omega_2 + \omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$7.2383443E-01$	$6.2205948E-00$	$5.6900988E-01$	$1.5790050E-01$	$1.3570573E-00$	$3.4448615E-02$
$\theta_{4,0,-12,0}$	$\cos(-8\omega_1 + 12\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$7.5137341E-01$	$9.4409336E-00$	$1.1993701E-02$	$-2.3719314E-01$	$-2.9803087E-00$	$7.4876998E-02$
$\theta_{4,0,-12,0}$	$\cos(-7\omega_1 + 11\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$9.7153658E-01$	$1.1252295E-01$	$1.3208611E-02$	$-3.7796270E-01$	$-4.3775480E-00$	$1.4704110E-01$
$\theta_{4,0,-10,0}$	$\cos(-6\omega_1 + 10\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.2082527E-00$	$1.2811895E-01$	$1.3814889E-02$	$-6.1234960E-01$	$-6.4931442E-00$	$3.1034239E-01$
$\theta_{4,0,-8,0}$	$\cos(-5\omega_1 + 9\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.4311361E-00$	$1.3784950E-01$	$1.3566077E-02$	$-1.0402000E-00$	$-1.0019386E-01$	$7.5605392E-01$
$\theta_{4,0,-8,0}$	$\cos(-4\omega_1 + 8\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.5918052E-00$	$1.3802992E-01$	$1.2314420E-02$	$-2.0446723E-00$	$-1.7729930E-01$	$2.6263796E-00$
$\theta_{4,0,-7,0}$	$\cos(-3\omega_1 + 7\omega_2 - 4\omega_3 + \omega_4)$	$\begin{matrix} & & & \\ 1 & 2 & 1 & 2 \end{matrix}$	$\begin{matrix} & & & \\ C & DC & DC^2 & \\ & & & \end{matrix}$	$1.6273816E-00$	$1.2576605E-01$	$1.0109781E-02$	$-8.9811641E-00$	$-6.9407538E-01$	$4.9565085E-01$

8 4, 0, -6, 0 )	COS ( -2L +6L -4W +0W ) 1 2 1 2						
8 4, 0, 0 )	C DC E.4769938E 00 1.0070063E 01 7.2736672E 01	<sup>2</sup> <sup>D C</sup>	C/N 3.5494864E 00	DC/N 2.4200204E 01	C/N=N 8.5300634E 00		
8 4, 0, -5, 0 )	COS ( -1L +5L -4W +0W ) 1 2 1 2						
8 4, 0, 0 )	C DC 1.1179434E 00 6.6850263E 00 4.3790766E 01	<sup>2</sup> <sup>D C</sup>	C/N 1.1031295E 00	DC/N 6.5964428E 00	C/N=N 1.0885119E 00		
8 4, 0, 2, 0 )	COS ( +5L -1L -4W +0W ) 1 2 1 2						
8 4, 0, 0 )	C DC -1.3383950E-02 -3.4738005E-02 -4.5063299E-02	<sup>2</sup> <sup>D C</sup>	C/N -2.9112541E-03	DC/N -7.5561520E-03	C/N=N -6.3325107E-04		
8 3, 1,-11, 0 )	COS ( -8L +12L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -5.2574157E 00 -6.0815870E 01 -7.1273624E 02	<sup>2</sup> <sup>D C</sup>	C/N 1.6595650E 00	DC/N 1.9198320E 01	C/N=N -5.2391992E-01		
8 3, 1,-10, 0 )	COS ( -7L +11L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -6.7647595E 00 -7.1607561E 01 -7.7035629E 02	<sup>2</sup> <sup>D C</sup>	C/N 2.6917350E 00	DC/N 2.7857919E 01	C/N=N -1.0238396E 00		
8 3, 1, -9, 0 )	COS ( -6L +10L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -8.3624256E 00 -8.0346748E 01 -7.8801105E 02	<sup>2</sup> <sup>D C</sup>	C/N 4.2381267E 00	DC/N 4.0720205E 01	C/N=N -2.1479076E 00		
8 3, 1, -8, 0 )	COS ( -5L +9L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -9.8297842E 00 -8.4910305E 01 -7.5348234E 02	<sup>2</sup> <sup>D C</sup>	C/N 7.1446326E 00	DC/N 6.1715792E 01	C/N=N -5.1929700E 00		
8 3, 1, -7, 0 )	COS ( -4L +8L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -1.0825047E 01 -8.3131288E 01 -6.6225564E 02	<sup>2</sup> <sup>D C</sup>	C/N 1.3904762E 01	DC/N 1.0678206E 02	C/N=N -1.7860654E 01		
8 3, 1, -6, 0 )	COS ( -3L +7L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -1.0917975E 01 -7.3592176E 01 -5.2277296E 02	<sup>2</sup> <sup>D C</sup>	C/N 6.0253924E 01	DC/N 4.0613916E 02	C/N=N -3.3252826E 02		
8 3, 1, -5, 0 )	COS ( -2L +6L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -9.7169706E 00 -5.6730344E 01 -3.5882915E 02	<sup>2</sup> <sup>D C</sup>	C/N -2.3351658E 01	DC/N -1.3633340E 02	C/N=N -5.6118309E 01		
8 3, 1, -4, 0 )	COS ( -1L +5L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -7.1314893E 00 -3.5792413E 01 -2.0506586E 02	<sup>2</sup> <sup>D C</sup>	C/N -7.0369896E 00	DC/N -3.5318126E 01	C/N=N -6.9437421E 00		
8 3, 1, -3, 0 )	COS ( +0L +4L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -3.7310773E 00 -1.6599025E 01 -9.3215072E 01	<sup>2</sup> <sup>D C</sup>	C/N -2.3163700E 00	DC/N -1.0305196E 01	C/N=N -1.4380753E 00		
8 3, 1, -2, 0 )	COS ( +4L +0L -3W -1W ) 1 2 1 2						
8 3, 1, 0 )	C DC -1.9008185E-02 -1.0855215E-01 -1.2054274E 00	<sup>2</sup> <sup>D C</sup>	C/N -4.7920462E-03	DC/N -2.7138037E-02	C/N=N -1.1880116E-03		
8 2, 2,-10, 0 )	COS ( -8L +12L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	C DC 1.3782584E 01 1.4568854E 02 1.5643753E 03	<sup>2</sup> <sup>D C</sup>	C/N -4.3508784E 00	DC/N -4.5990878E 01	C/N=N 1.3734829E 00		

8 2, 2, -9, 0 )	COS ( -7L +11L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	1.7644293E 01	DC	D C	C/N	DC/N	C/N/N	
		1.6919048E 02	1.6548548E 03	-6.8642651E 00	-6.5821287E 01	2.6704462E 00	
8 2, 2, -8, 0 )	COS ( -6L +10L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	2.1674675E 01	DC	D C	C/N	DC/N	C/N/N	
		1.8667770E 02	1.6497558E 03	-1.0984853E 01	-9.4609358E 01	5.5671884E 00	
8 2, 2, -7, 0 )	COS ( -5L +9L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	2.5275182E 01	DC	D C	C/N	DC/N	C/N/N	
		1.9321141E 02	1.5290737E 03	-1.8370890E 01	-1.4043285E 02	1.3352609E 01	
8 2, 2, -6, 0 )	COS ( -4L +8L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	2.7543829E 01	DC	D C	C/N	DC/N	C/N/N	
		1.8422346E 02	1.2937957E 03	-3.5380023E 01	-2.3663486E 02	4.5445606E 01	
8 2, 2, -5, 0 )	COS ( -3L +7L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	2.7303492E 01	DC	D C	C/N	DC/N	C/N/N	
		1.5756125E 02	9.7508136E 02	-1.5112352E 02	-8.6954614E 02	8.3401772E 02	
8 2, 2, -4, 0 )	COS ( -2L +6L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	2.3865768E 01	DC	D C	C/N	DC/N	C/N/N	
		1.1600792E 02	6.3386416E 02	5.7353809E 01	2.7878827E 02	1.3783170E 02	
8 2, 2, -3, 0 )	COS ( -1L +5L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	1.6940471E 01	DC	D C	C/N	DC/N	C/N/N	
		6.8843749E 01	3.4309267E 02	1.6715992E 01	6.7931497E 01	1.6494468E 01	
8 2, 2, -2, 0 )	COS ( -4L +4L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	8.3382445E 00	DC	D C	C/N	DC/N	C/N/N	
		2.9768669E 01	1.5302592E 02	5.1747818E 00	1.8481325E 01	3.2126672E 00	
8 2, 2, -1, 0 )	COS ( -3L +3L -2W -2W ) 1 2 1 2						
8 2, 2, 0 )	1.5363094E 00	DC	D C	C/N	DC/N	C/N/N	
		8.5921242E 00	6.0408233E 01	6.9581045E-01	3.8912676E 00	3.1512335E-01	
8 1, 3, -10, 0 )	COS ( -9L +13L -1W -3W ) 1 2 1 2						
8 1, 3, 0 )	-1.2171057E 01	DC	D C	C/N	DC/N	C/N/N	
		-1.2850315E 02	-1.3776624E 03	3.2326117E 00	3.4130215E 01	-8.5857611E-01	
8 1, 3, -8, 0 )	COS ( -8L +12L -1W -3W ) 1 2 1 2						
8 1, 3, 0 )	-1.6042579E 01	DC	D C	C/N	DC/N	C/N/N	
		-1.5358274E 02	-1.4988763E 03	5.0643123E 00	4.8462913E 01	-1.5986993E 00	
8 1, 3, -6, 0 )	COS ( -7L +11L -1W -3W ) 1 2 1 2						
8 1, 3, 0 )	-2.0426614E 01	DC	D C	C/N	DC/N	C/N/N	
		-1.7553896E 02	-1.5462702E 03	7.9475440E 00	6.8290973E 01	-3.0918807E 00	
8 1, 3, -4, 0 )	COS ( -6L +10L -1W -3W ) 1 2 1 2						
8 1, 3, 0 )	-2.4930109E 01	DC	D C	C/N	DC/N	C/N/N	
		-1.8990769E 02	-1.4953708E 03	1.2634724E 01	9.6246336E 01	-6.4033527E 00	
8 1, 3, -2, 0 )	COS ( -5L +9L -1W -3W ) 1 2 1 2						
8 1, 3, 0 )	-2.8827063E 01	DC	D C	C/N	DC/N	C/N/N	
		-1.9172765E 02	-1.3353901E 03	2.0952522E 01	1.3935439E 02	-1.5229029E 01	

8 16 3, -5, 0 1	COS ( -4L +8L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-3.1065563E 01	DC	2 D C	C/N	DC/N	C/N+N	
	-1.7700829E 02	-1.0792690E 03	3.9903686E 01	2.2736698E 02	-5.1256248E 01		
8 16 3, -4, 0 1	COS ( -3L +7L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-3.0410197E 01	DC	2 D C	C/N	DC/N	C/N+N	
	-1.4501313E 02	-7.6934183E 02	1.6782724E 02	8.0029581E 02	-9.2620193E 02		
8 16 3, -3, 0 1	COS ( -2L +6L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-2.5903824E 01	DC	2 D C	C/N	DC/N	C/N+N	
	-1.0066787E 02	-4.6974539E 02	-6.2251629E 01	-2.4192331E 02	-1.4960206E 02		
8 16 3, -2, 0 1	COS ( -1L +5L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-1.7715243E 01	DC	2 D C	C/N	DC/N	C/N+N	
	-5.5209925E 01	-2.4181668E 02	-1.7480497E 01	-5.4478335E 01	-1.7248862E 01		
8 16 3, -1, 0 1	COS ( +0L +4L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-3.0769534E 00	DC	2 D C	C/N	DC/N	C/N+N	
	-1.7789883E 01	-1.0554676E 02	-2.9365203E 00	-1.1044518E 01	-1.4509853E 00		
8 16 3, 0, 0 1	COS ( +1L +3L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-1.5278281E 00	DC	2 D C	C/N	DC/N	C/N+N	
	-7.3569341E 00	-4.8358768E 01	-6.9193314E-01	-3.3318582E 00	-3.1336737E-01		
8 16 3, 1, 0 1	COS ( +2L +2L -1W -3W ) 1 2 1 2						
8 16 3, 0 3	-3.5280181E-01	DC	2 D C	C/N	DC/N	C/N+N	
	-2.4195090E 00	-2.0037667E 01	-1.2568810E-01	-8.6245580E-01	-4.4602655E-02		
8 06 4, -10, 0 1	COS ( -10L +14L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	3.9486266E 00	DC	2 D C	C/N	DC/N	C/N+N	
	4.1617001E 01	4.4558943E 02	-9.0446259E-01	-9.5399352E 00	2.0733148E-01		
8 06 4, -9, 0 1	COS ( -9L +13L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	5.3308234E 00	DC	2 D C	C/N	DC/N	C/N+N	
	5.0965775E 01	4.9648335E 02	-1.4158579E 00	-1.3536422E 01	3.7604932E-01		
8 06 4, -8, 0 1	COS ( -8L +12L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	6.9943367E 00	DC	2 D C	C/N	DC/N	C/N+N	
	5.9988875E 01	5.2703982E 02	-2.2080314E 00	-1.8937255E 01	6.9703014E-01		
8 06 4, -7, 0 1	COS ( -7L +11L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	8.0573134E 00	DC	2 D C	C/N	DC/N	C/N+N	
	6.7285876E 01	5.2772597E 02	-3.4498138E 00	-2.6176628E 01	1.3403456E 00		
8 06 4, -6, 0 1	COS ( -6L +10L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	1.0733529E 01	DC	2 D C	C/N	DC/N	C/N+N	
	7.1085764E 01	4.9198009E 02	-5.4398157E 00	-3.6026683E 01	2.7569306E 00		
8 06 4, -5, 0 1	COS ( -5L +9L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	1.2299483E 01	DC	2 D C	C/N	DC/N	C/N+N	
	6.9592319E 01	4.1978520E 02	-8.9398420E 00	-5.0582143E 01	6.49777913E 00		
8 06 4, -4, 0 1	COS ( -4L +8L +0W -4W ) 1 2 1 2						
8 06 4, 0 3	1.3095008E 01	DC	2 D C	C/N	DC/N	C/N+N	
	6.1654124E 01	3.2061001E 02	-1.6820525E 01	-7.9194663E 01	2.1605949E 01		

$\theta_{0,4,-3,0}$	$\cos(-3L_1 + 7L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$1.2600542E\ 01$	$4.7691556E\ 01$	$2.1357681E\ 02$	$-6.9539644E\ 01$	$-2.6319929E\ 02$	$3.8377412E\ 02$	
$\theta_{0,4,-2,0}$	$\cos(-2L_1 + 6L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$1.0454467E\ 01$	$3.0480633E\ 01$	$1.2176829E\ 02$	$2.5123998E\ 01$	$7.3250540E\ 01$	$6.0377566E\ 01$	
$\theta_{0,4,-1,0}$	$\cos(-1L_1 + 5L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$2.3874160E\ 00$	$1.0462719E\ 01$	$5.6662525E\ 01$	$2.3557802E\ 00$	$1.0324077E\ 01$	$2.3245637E\ 00$	
$\theta_{0,4,-6,0}$	$\cos(+0L_1 + 6L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$2.7775516E\ 00$	$5.5463970E\ 00$	$3.0013350E\ 01$	$1.7243914E\ 00$	$3.4433776E\ 00$	$1.0705564E\ 00$	
$\theta_{0,4,1,0}$	$\cos(+1L_1 + 3L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$3.9898952E-01$	$2.1146991E\ 00$	$1.4111253E\ 01$	$1.8069708E-01$	$9.5771924E-01$	$8.1835316E-02$	
$\theta_{0,4,2,0}$	$\cos(+2L_1 + 2L_2 + 0W_1 - 4W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{0,4,0}$	$1.2562915E-01$	$8.0591017E-01$	$6.3444500E\ 00$	$4.4781645E-02$	$2.0727395E-01$	$1.5962821E-02$	
$\theta_{-1,3,-3,0}$	$\cos(-4L_1 + 6L_2 + 1W_1 - 3W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,3,0}$	$6.2546247E\ 00$	$1.7227327E\ 01$	$3.0897055E\ 01$	$-3.9489129E\ 00$	$-1.0876624E\ 01$	$2.4931812E\ 00$	
$\theta_{-1,3,-2,0}$	$\cos(-3L_1 + 5L_2 + 1W_1 - 3W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,3,0}$	$3.2726320E\ 00$	$2.5605181E\ 00$	$-3.1221051E\ 01$	$-3.3171784E\ 00$	$-2.5953714E\ 00$	$3.3623311E\ 00$	
$\theta_{-1,3,-1,0}$	$\cos(-2L_1 + 4L_2 + 1W_1 - 3W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,3,0}$	$-1.3129717E\ 00$	$-7.6368710E\ 00$	$-5.4693254E\ 01$	$3.3730218E\ 00$	$1.9619107E\ 01$	$-8.6652865E\ 00$	
$\theta_{-1,3,-6,0}$	$\cos(-1L_1 + 3L_2 + 1W_1 - 3W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{1,3,0}$	$-1.5278281E\ 00$	$-7.3569341E\ 00$	$-4.0358768E\ 01$	$-7.3433011E\ 00$	$-3.5360118E\ 01$	$-3.5294593E\ 01$	
$\theta_{-2,2,-2,0}$	$\cos(+0L_1 + 0L_2 + 2W_1 - 2W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{2,2,0}$	$4.1483294E-01$	$3.0020711E\ 00$	$2.5599630E\ 01$				
$\theta_{4,2,0}$	$1.4519402E\ 00$	$1.5422114E\ 01$	$1.8676608E\ 02$				
$\theta_{2,4,0}$	$3.5915986E\ 00$	$3.3489358E\ 01$	$3.6587317E\ 02$				
$\theta_{2,2,1}$	$-2.6942569E\ 01$	$-2.6945226E\ 02$	$-3.1110389E\ 03$				
$\theta_{-3,1,-4,0}$	$\cos(+1L_1 - 3L_2 + 3W_1 - 1W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{3,1,0}$	$1.1234797E\ 00$	$4.0148945E\ 00$	$9.3469769E\ 00$	$-5.4008158E\ 00$	$-1.9297052E\ 01$	$2.5958297E\ 01$	
$\theta_{-3,1,-5,0}$	$\cos(+2L_1 - 4L_2 + 3W_1 - 1W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{3,1,0}$	$1.9183929E\ 00$	$9.6205090E\ 00$	$4.5910349E\ 01$	$4.9282449E\ 00$	$2.4715069E\ 01$	$1.2660652E\ 01$	
$\theta_{-3,1,-6,0}$	$\cos(+3L_1 - 5L_2 + 3W_1 - 1W_2)$	$C$	$DC$	$D_C$	$C/N$	$DC/N$	$C/N+N$
$\theta_{3,1,0}$	$2.4253357E\ 00$	$1.4976191E\ 01$	$9.2050501E\ 01$	$2.4583489E\ 00$	$1.5180043E\ 01$	$2.4918114E\ 00$	

8 2, 0, -7, 1 )	COS ( -4L +8L -2W +0W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 2, 0, 1 )	2.1852112E 00	2.1421179E 01	2.2208646E 02	-2.8069017E 00	-2.7515485E 01	3.6054626E 00	
8 2, 0, -6, 1 )	COS ( -3L +7L -2W +0W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 2, 0, 1 )	2.7249071E 00	2.4260687E 01	2.3202303E 02	-1.5038168E 01	-1.3388944E 02	8.2992365E 01	
8 2, 0, -5, 1 )	COS ( -2L +6L -2W +0W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 2, 0, 1 )	3.1673349E 00	2.5496381E 01	2.2540003E 02	7.6116833E 00	6.1272469E 01	1.8292273E 01	
8 1, 1, -6, 1 )	COS ( -4L +8L -1W -1W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 1, 1, 1 )	-8.1024656E 00	-7.1368377E 01	-6.7360819E 02	1.0407609E 01	9.1672614E 01	-1.3368565E 01	
8 1, 1, -5, 1 )	COS ( -3L +7L -1W -1W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 1, 1, 1 )	-8.0127373E 01	-8.0110443E 01	-6.9341364E 02	5.5890772E 01	4.4211206E 02	-3.0844898E 02	
8 1, 1, -4, 1 )	COS ( -2L +6L -3W -1W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 1, 1, 1 )	-1.1812567E 01	-8.3385271E 01	-6.6402153E 02	-2.8307760E 01	-2.0039007E 02	-6.8220982E 01	
8 0, 2, -5, 1 )	COS ( -4L +8L +0W -2W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 0, 2, 1 )	7.5644093E 00	5.9088970E 01	5.0360009E 02	-9.7164767E 00	-7.5899726E 01	1.2400809E 01	
8 0, 2, -4, 1 )	COS ( -3L +7L +0W -2W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 0, 2, 1 )	9.5032996E 00	6.5699121E 01	5.1027536E 02	-5.2445698E 01	-3.4257912E 02	2.8943637E 02	
8 0, 2, -3, 1 )	COS ( -2L +6L +0W -2W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 0, 2, 1 )	1.1174763E 01	6.7728968E 01	4.8176439E 02	2.6855049E 01	1.6276511E 02	6.4537598E 01	
8-16 1, 0, 1 )	COS ( +0L +2L +1W -1W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 1, 1, 1 )	-8.2707797E 00	-4.0148566E 01	-3.5220522E 02	-1.0276965E 01	-5.9784208E 01	-1.2760526E 01	
8-26 0, 1, 1 )	COS ( +0L +0L +2W +0W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 26 0, 1 )	4.8328045E 00	2.4390954E 01	1.7519700E 02				
8-16-1, 0, 1 )	COS ( +0L +0L +1W +1W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 16 1, 1 )	-4.1603790E 00	-2.7390655E 01	-2.2188469E 02				
8 06-2, -2, 1 )	COS ( +0L +0L +0W +2W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 06 2, 1 )	9.5969281E-01	7.4698741E 00	6.7981411E 01				
8 56 0, -8, 0 )	COS ( -4L +9L -5W +0W )	1    2    1    2	C    DC	D C	C/N	DC/N	C/N+N
8 56 0, 0 )	-2.4277200E 00	-2.3658250E 01	-2.3459916E 02	6.4596602E 00	6.2949706E 01	-1.7187818E 01	

8 5. 0. -8. 0. 1	$\cos(-3L_1 + 8L_2 - 5W_1 + 0W_2)$	1 2 1 2	C DC DC	2	C/N -1.0062452E 01	DC/N -8.8728130E 01	C/N=0 -4.5431470E 01
8 4. 1. -9. 0. 1	$\cos(-5L_1 + 10L_2 - 4W_1 - 1W_2)$	1 2 1 2	C DC DC	2	C/N -2.1053729E 01	DC/N -2.0427380E 02	C/N=0 2.1634796E 01
8 4. 1. -8. 0. 1	$\cos(-4L_1 + 9L_2 - 4W_1 - 1W_2)$	1 2 1 2	C DC DC	2	C/N -5.4364896E 01	DC/N -4.7600929E 02	C/N=0 1.4465373E 02
8 4. 1. -7. 0. 1	$\cos(-3L_1 + 8L_2 - 4W_1 - 1W_2)$	1 2 1 2	C DC DC	2	C/N 8.3497972E 01	DC/N 6.5409636E 02	C/N=0 3.7698918E 02
8 4. 1. -6. 0. 1	$\cos(-2L_1 + 7L_2 - 4W_1 - 1W_2)$	1 2 1 2	C DC DC	2	C/N 1.7874304E 01	DC/N 1.2435732E 02	C/N=0 2.1829883E 01
8 3. 2. -8. 0. 1	$\cos(-5L_1 + 10L_2 - 3W_1 - 2W_2)$	1 2 1 2	C DC DC	2	C/N 7.1528742E 01	DC/N 6.2306771E 02	C/N=0 -7.3502882E 01
8 3. 2. -7. 0. 1	$\cos(-4L_1 + 9L_2 - 3W_1 - 2W_2)$	1 2 1 2	C DC DC	2	C/N 1.8268260E 02	DC/N 1.4189632E 03	C/N=0 -4.8608058E 02
8 3. 2. -6. 0. 1	$\cos(-3L_1 + 8L_2 - 3W_1 - 2W_2)$	1 2 1 2	C DC DC	2	C/N -2.7647744E 02	DC/N -1.8941409E 03	C/N=0 -1.2482818E 03
8 3. 2. -5. 0. 1	$\cos(-2L_1 + 7L_2 - 3W_1 - 2W_2)$	1 2 1 2	C DC DC	2	C/N -5.7968663E 01	DC/N -3.4699116E 02	C/N=0 -7.0797045E 01
8 2. 3. -7. 0. 1	$\cos(-5L_1 + 10L_2 - 2W_1 - 3W_2)$	1 2 1 2	C DC DC	2	C/N -1.2131841E 02	DC/N -9.3651693E 02	C/N=0 1.2466670E 02
8 2. 3. -6. 0. 1	$\cos(-4L_1 + 9L_2 - 2W_1 - 3W_2)$	1 2 1 2	C DC DC	2	C/N -3.0631784E 02	DC/N -2.0767697E 03	C/N=0 8.1504834E 02
8 2. 3. -5. 0. 1	$\cos(-3L_1 + 8L_2 - 2W_1 - 3W_2)$	1 2 1 2	C DC DC	2	C/N 4.5650168E 02	DC/N 2.6795900E 03	C/N=0 2.0610823E 03
8 2. 3. -4. 0. 1	$\cos(-2L_1 + 7L_2 - 2W_1 - 3W_2)$	1 2 1 2	C DC DC	2	C/N 9.3645029E 01	DC/N 4.6986708E 02	C/N=0 1.1436854E 02
8 1. 4. -6. 0. 1	$\cos(-5L_1 + 10L_2 - 1W_1 - 4W_2)$	1 2 1 2	C DC DC	2	C/N 1.0270244E 02	DC/N 6.9106936E 02	C/N=0 -1.0553695E 02

8 1, 4, -5, 0 1	COS ( -4L +9L -1W -4W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 1, 4, 0 1	-9.6294578E 01 -5.5785319E 02 -3.4907157E 03			C/N 2.5621993E 02	DC/N 1.4843319E 03	C/N=0 -6.8174819E 02
8 1, 4, -4, 0 1	COS ( -3L +8L -1W -4W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 1, 4, 0 1	-8.3207093E 01 -4.0692590E 02 -2.2478892E 03			C/N -3.7567588E 02	DC/N -1.0372502E 03	C/N=0 -1.6961579E 03
8 1, 4, -3, 0 1	COS ( -2L +7L -1W -4W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 1, 4, 0 1	-6.1647406E 01 -2.4986308E 02 -1.2458123E 03			C/N -7.3289889E 01	DC/N -3.0515742E 02	C/N=0 -9.1951435E 01
8 0, 5, -6, 0 1	COS ( -5L +10L +0W -5W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 0, 5, 0 1	3.3773080E 01 1.9381952E 02 1.1954442E 03			C/N -3.4705191E 01	DC/N -1.9916879E 02	C/N=0 3.5663028E 01
8 0, 5, -4, 0 1	COS ( -4L +9L +0W -5W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 0, 5, 0 1	3.2126940E 01 1.5445872E 02 8.3092312E 02			C/N -8.5483134E 01	DC/N -4.1098267E 02	C/N=0 2.2745292E 02
8 0, 5, -3, 0 1	COS ( -3L +8L +0W -5W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 0, 5, 0 1	2.72726612E 01 1.0674607E 02 5.0482001E 02			C/N 1.2315254E 02	DC/N 4.8195317E 02	C/N=0 5.5602759E 02
8 0, 5, -2, 0 1	COS ( -2L +7L +0W -5W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 0, 5, 0 1	1.9693220E 01 6.0929531E 01 2.6622893E 02			C/N 2.4051313E 01	DC/N 7.4413150E 01	C/N=0 2.9373035E 01
8-16 41 -2, 0 1	COS ( -2L +5L +1W -4W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 16 4, 0 1	-2.0843949E 00 -1.7868544E 01 -1.3081307E 02			C/N -2.1177636E 02	DC/N -1.3305944E 03	C/N=0 -1.5770085E 04
8-4, 1, 6, 0 1	COS ( -4L -5L +4W -1W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 4, 1, 0 1	-3.0884348E 00 -1.9016911E 01 -1.1482982E 02			C/N 2.2998256E 02	DC/N 1.4161084E 03	C/N=0 -1.7125822E 04
8-1, 2, -2, 1 1	COS ( -2L +5L +1W -2W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 16 2, 1 1	-1.9696369E 01 -1.4656018E 02 -1.3116779E 03			C/N -1.4467048E 03	DC/N -1.0914308E 04	C/N=0 -1.0921926E 05
8 26 1, -6, 1 1	COS ( -2L +5L -2W +1W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 26 1, 1 1	-4.6721512E 00 -2.7530079E 01 -1.2864344E 02			C/N -3.4791522E 02	DC/N -2.0500478E 03	C/N=0 -2.5907766E 04
8 66 0, -16, 0 1	COS ( -4L +10L -6W +0W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 6, 0, 0 1	3.4880592E 00 3.7713910E 01 4.1786524E 02			C/N 1.2979600E 02	DC/N 1.4041972E 03	C/N=0 4.8326778E 03
8 56 1, -8, 0 1	COS ( -4L +10L -3W -1W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 56 1, 0 1	-3.48892466E 01 -3.4305296E 02 -3.4734020E 03			C/N -1.2991467E 03	DC/N -1.2772847E 04	C/N=0 -4.8370962E 04
8 46 2, -8, 0 1	COS ( -4L +10L -4W -2W ) 1 2 1 2					
	<sup>2</sup> C DC D C					
8 46 2, 0 1	1.4529178E 02 1.2852356E 03 1.1796784E 04			C/N 5.4096302E 03	DC/N 4.7853014E 04	C/N=0 2.0141607E 05

$\{ 3, 3, -7, 0 \}$	$\cos (-4L_1 + 10L_2 - 3W_1 - 3W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 3, 3, 0 \}$	$-3.2213608E\ 02$	$-2.5323508E\ 03$	$-2.0876353E\ 04$	$-1.1994051E\ 04$	$-9.4286693E\ 04$	$-4.4657298E\ 05$
$\{ 2, 4, -6, 0 \}$	$\cos (-4L_1 + 10L_2 - 2W_1 - 4W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 2, 4, 0 \}$	$4.0105143E\ 02$	$2.7582437E\ 03$	$2.0204627E\ 04$	$1.4932297E\ 04$	$1.0269733E\ 05$	$5.5597228E\ 05$
$\{ 1, 5, -5, 0 \}$	$\cos (-4L_1 + 10L_2 - 1W_1 - 5W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 1, 5, 0 \}$	$-2.6577516E\ 02$	$-1.5668197E\ 03$	$-1.0075156E\ 04$	$-9.8955725E\ 03$	$-5.8337197E\ 04$	$-3.6844058E\ 05$
$\{ 0, 6, -4, 0 \}$	$\cos (-4L_1 + 10L_2 + 0W_1 - 6W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 0, 6, 0 \}$	$7.3216915E\ 01$	$3.5983163E\ 02$	$2.0053742E\ 03$	$2.7260760E\ 03$	$1.3397565E\ 04$	$1.0149964E\ 05$
$\{ -3, 3, 3, 0 \}$	$\cos (+0L_1 + 0L_2 + 3W_1 - 3W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 3, 3, 0 \}$	$-6.7513727E-01$	$-6.9865264E\ 00$	$-8.2315120E\ 01$			
$\{ 4, 0, -9, 1 \}$	$\cos (-4L_1 + 10L_2 - 4W_1 + 0W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 4, 0, 1 \}$	$1.1168608E\ 01$	$1.3614258E\ 02$	$1.7387135E\ 03$	$4.1583936E\ 02$	$5.0689793E\ 03$	$1.5482894E\ 04$
$\{ 3, 1, -8, 1 \}$	$\cos (-4L_1 + 10L_2 - 3W_1 - 1W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 3, 1, 1 \}$	$-8.0299606E\ 01$	$-8.9996647E\ 02$	$-1.0660414E\ 04$	$-2.9897850E\ 03$	$-3.3508337E\ 04$	$-1.1131828E\ 05$
$\{ 2, 2, -7, 1 \}$	$\cos (-4L_1 + 10L_2 - 2W_1 - 2W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 2, 2, 1 \}$	$2.1752003E\ 02$	$2.2240979E\ 03$	$2.4307678E\ 04$	$8.0988953E\ 03$	$8.2809551E\ 04$	$3.0154513E\ 05$
$\{ 1, 3, -6, 1 \}$	$\cos (-4L_1 + 10L_2 - 1W_1 - 3W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 1, 3, 1 \}$	$-2.6342615E\ 02$	$-2.4342373E\ 03$	$-2.4404304E\ 04$	$-9.8081124E\ 03$	$-9.0633647E\ 04$	$-3.6518420E\ 05$
$\{ 0, 4, -5, 1 \}$	$\cos (-4L_1 + 10L_2 + 0W_1 - 4W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 0, 4, 1 \}$	$1.2053399E\ 02$	$9.9491875E\ 02$	$9.0911410E\ 03$	$4.4878267E\ 03$	$3.7043683E\ 04$	$1.6709468E\ 05$
$\{ -3, 1, 2, 1 \}$	$\cos (+0L_1 + 0L_2 + 3W_1 - 1W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 3, 1, 1 \}$	$-1.8504884E\ 01$	$-1.6365791E\ 02$	$-1.7302701E\ 03$			
$\{ 1, -3, -2, 1 \}$	$\cos (+0L_1 + 0L_2 - 1W_1 + 3W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 1, 3, 1 \}$	$-4.4818550E\ 00$	$-4.9707600E\ 01$	$-6.2127441E\ 02$			
$\{ 1, 1, -7, 2 \}$	$\cos (-4L_1 + 10L_2 - 1W_1 - 1W_2)$	$\begin{matrix} C \\ DC \end{matrix}$	$\begin{matrix} DC \\ DC \end{matrix}$	$C/N$	$DC/N$	$C/N=N$
$\{ 1, 1, 2 \}$	$-2.7867894E\ 01$	$-3.4196674E\ 02$	$-4.4769826E\ 03$	$-1.0375943E\ 03$	$-1.2732478E\ 04$	$-3.8632617E\ 04$

## Appendix II

## SAO ANALYTICAL DEVELOPMENT OF THE PLANETARY DISTURBING FUNCTION

## CONVENTIONAL RELATIVE COORDINATES, INNER PLANET

ALPHA = .5454323      BETA = .4026858

 E<sub>1</sub> = .04823880      E<sub>2</sub> = .05599560      NU = 1.1967703E-04

 $(J_1, J_2, K_1, L_1) \cos(I_1 L_1 + I_2 L_2 - J_1 W_1 - J_2 W_2)$ 

C	DC	D <sup>2</sup> C	C/N	DC/N	C/N+N
(S <sub>1</sub> , S <sub>2</sub> , S <sub>1</sub> )	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---	X.XXXXXXXE---

 $(L_0, O_1, O_2, O_3) \cos(I_0 O_1 + O_1 L_1 + O_2 W_1 + O_3 W_2)$ 

C	DC	D <sup>2</sup> C	
(0, 0, 0, 0)	1.0901656E 00	2.2065981E-01	6.4855371E-01
(2, 0, 0, 0)	5.0566100E-04	1.8253456E-03	8.9310901E-03
(0, 2, 0, 0)	6.8135631E-04	2.4595741E-03	1.2034257E-02
(4, 0, 0, 0)	6.44957340E-07	5.0560257E-06	4.6013595E-05
(2, 2, 0, 0)	8.4317204E-06	5.2392908E-05	4.1557170E-04
(0, 4, 0, 0)	5.5694967E-06	2.9974673E-05	2.1530508E-04
(6, 0, 0, 0)	3.1903996E-09	1.4475753E-08	1.9476314E-07
(4, 2, 0, 0)	4.90032291E-08	4.1654135E-07	4.9728651E-06
(2, 4, 0, 0)	1.4269038E-07	1.25338550E-06	1.3306912E-05
(0, 6, 0, 0)	5.1950744E-08	3.8995840E-07	3.7190981E-06
(0, 0, 1, 1)	-1.0402490E-04	-3.7551122E-04	-1.8373094E-03
(2, 0, 1, 1)	-1.2872983E-06	-7.9989966E-06	-6.3446689E-05
(0, 2, 1, 1)	-1.7345787E-06	-1.0778301E-05	-8.5491666E-05
(4, 0, 1, 1)	-6.1118609E-09	-6.3594730E-08	-7.5922359E-07
(2, 2, 1, 1)	-5.6004616E-08	-5.2916167E-07	-5.9103240E-06
(0, 4, 1, 1)	-2.9354353E-08	-2.5794383E-07	-2.7375063E-06
(0, 0, 2, 2)	5.9981256E-08	3.8891960E-07	3.1531312E-06
(2, 0, 2, 2)	2.0605719E-09	1.9718563E-08	2.2179056E-07
(0, 2, 2, 2)	2.7765314E-09	2.6569909E-08	2.9885318E-07
(0, 0, 3, 1)	-4.2314652E-11	-4.1969405E-10	-4.8180831E-09

 $(-1, 1, 1, 0) \cos(I_0 O_1 + O_1 L_1 + O_1 W_1 - I_1 W_2)$ 

C	DC	D <sup>2</sup> C	
(1, 1, 1, 0)	-7.6746669E-04	-3.4648626E-03	-1.9010860E-02
(3, 1, 0, 1)	-4.5219126E-06	-3.1981862E-05	-2.7364370E-04
(1, 2, 0, 1)	-1.2126700E-05	-7.5614528E-05	-5.8580624E-04
(5, 1, 0, 1)	-1.3653013E-08	-1.5444434E-07	-1.9628577E-06
(3, 3, 0, 1)	-1.4840086E-07	-1.4321933E-06	-1.6188544E-05
(1, 5, 0, 1)	-1.6469622E-07	-1.3740843E-06	-1.3947969E-05
(1, 1, 1, 1)	2.5979774E-06	1.7294322E-05	1.4118078E-04
(3, 1, 1, 1)	3.6035192E-08	3.6033505E-07	4.1820418E-06
(1, 3, 1, 1)	7.7705589E-08	7.2042917E-07	7.9092686E-06
(1, 1, 2, 1)	-4.5110169E-09	-4.3972330E-08	-5.0013851E-07

 $(-2, 2, 2, 0) \cos(I_0 O_1 + O_1 L_1 + O_2 W_1 - 2W_2)$ 

C	DC	D <sup>2</sup> C	
(2, 2, 2, 0)	3.0267324E-06	2.1903916E-05	1.8678322E-04
(4, 2, 0, 0)	2.4651452E-08	2.6184103E-07	3.1709675E-06
(2, 4, 0, 0)	8.2166800E-08	7.6615283E-07	8.3702639E-06
(2, 2, 2, 1)	-2.3526137E-08	-2.3528457E-07	-2.7165442E-06







( 4, 0, -9, 1 )	COS ( -4L +10L -4W +0W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 4, 0, 1 )	7.2376212E-09	8.8224819E-08	1.1267429E-06	2.6947743E-07	3.2848634E-06	1.0033419E-05	
( 3, 1, -8, 1 )	COS ( -4L +10L -3W -1W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 3, 1, 1 )	-6.0404268E-08	-6.7698733E-07	-8.0191489E-06	-2.2490244E-06	-2.5206183E-05	-8.3737637E-05	
( 2, 2, -7, 1 )	COS ( -4L +10L -2W -2W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 2, 2, 1 )	1.8993756E-07	1.9420728E-06	2.1225361E-05	7.0719210E-06	7.2308949E-05	2.6330793E-04	
( 4, 2, 1 )	8.2891501E-11	6.7328142E-09	1.6083836E-07	3.0862887E-09	2.5068201E-07	1.1491139E-07	
( 2, 4, 1 )	-9.3122712E-09	-8.4814880E-08	-7.7482243E-07	-3.4672260E-07	-3.1579016E-06	-1.2909478E-05	
( 2, 2, 2 )	-5.3777348E-10	-6.9075933E-09	-9.6213090E-08	-2.0022852E-08	-2.5718954E-07	-7.4550827E-07	
( 1, 3, -6, 1 )	COS ( -4L +10L -1W -3W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 1, 3, 1 )	-2.6701024E-07	-2.4673567E-06	-2.4736340E-05	-9.9415580E-06	-9.1866776E-05	-3.7015276E-04	
( 3, 3, 1 )	-8.6780035E-10	-2.0426637E-08	-3.7567370E-07	-3.2310700E-08	-7.6054237E-07	-1.2030202E-06	
( 1, 5, 1 )	8.7003406E-09	6.9490669E-08	5.4857628E-07	3.2393867E-07	2.5873372E-06	1.2061167E-05	
( 1, 3, 2 )	6.8045601E-10	8.1297023E-09	1.0674388E-07	2.5335332E-08	3.0269217E-07	9.4330716E-07	
( 0, 4, -5, 1 )	COS ( -4L +10L +0W -4W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 0, 4, 1 )	1.4181951E-07	1.1706149E-06	1.0696577E-05	5.2803475E-06	4.3585354E-05	1.9660250E-04	
( 2, 4, 1 )	1.6235024E-09	2.6554233E-08	4.0967333E-07	6.0447657E-08	9.8869035E-07	2.2506399E-06	
( 0, 6, 1 )	-3.2380448E-09	-2.2129216E-08	-1.4467557E-07	-1.2056171E-07	-8.2393426E-07	-4.4888587E-06	
( 0, 4, 2 )	-3.2065727E-10	-3.5487649E-09	-4.3881078E-08	-1.1938991E-08	-1.3213071E-07	-4.4452294E-07	
( 5, 4, -11, 0 )	COS ( -6L +15L -5W -4W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 5, 4, 0 )	-3.3249973E-08	-3.9646430E-07	-4.8390752E-06	-8.2532800E-07	-9.8410031E-06	-2.0486221E-05	
( 4, 5, -10, 0 )	COS ( -6L +15L -4W -5W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 4, 5, 0 )	6.4147801E-08	7.0164095E-07	7.8942178E-06	1.5922712E-06	1.7416072E-05	3.9523221E-05	
( 3, 6, -9, 0 )	COS ( -6L +15L -3W -6W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 3, 6, 0 )	-8.2445754E-08	-8.2057314E-07	-8.4552188E-06	-2.0464615E-06	-2.0368196E-05	-5.0797092E-05	
( 2, 7, -8, 0 )	COS ( -6L +15L -2W -7W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 2, 7, 0 )	6.8072283E-08	6.1053009E-07	5.7186769E-06	1.6896844E-06	1.5154526E-05	4.1941202E-05	
( 1, 8, -7, 0 )	COS ( -6L +15L -1W -8W )	1 2 1 2					
	C DC		D C		C/N	DC/N	C/N=N
( 1, 8, 0 )	-3.2764451E-08	-2.6165273E-07	-2.2090167E-06	-8.1327641E-07	-6.4947217E-06	-2.0187078E-05	

- p. 3 In line 5 from bottom, the words "inner" and "outer"  
should be transposed.
- p. 7 The superscripts  $h$  on the right side of equation (16)  
should read  $h-1$ .
- p. 76 The first number of line 4 should read 0.11279093.
- p. 77 The  $a$  in line 16 should read  $+$ .
- p. 88 Erase the first  $\sum_{5,4}^{n,k}$  at top of page, and the  $\sum_{6,3}^{n,k}$ .